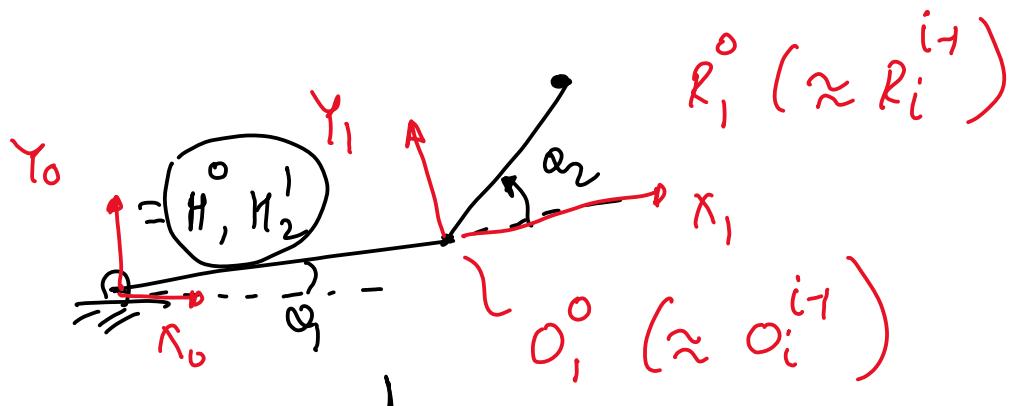


3D Manipulator Forward Kinematics

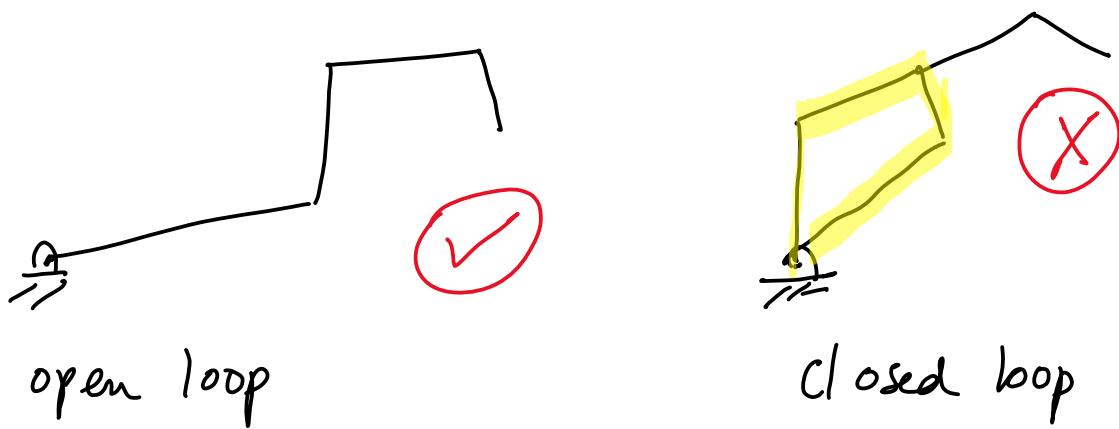
2D



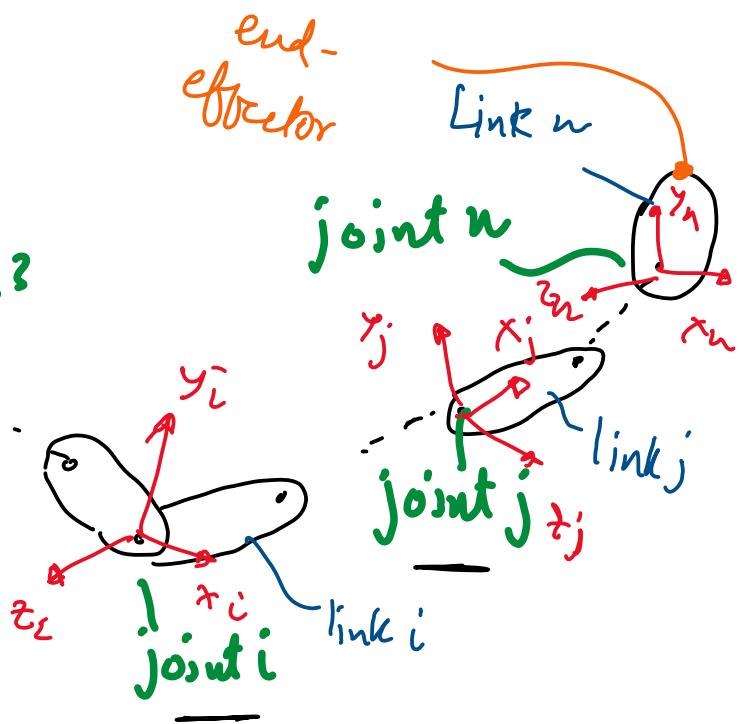
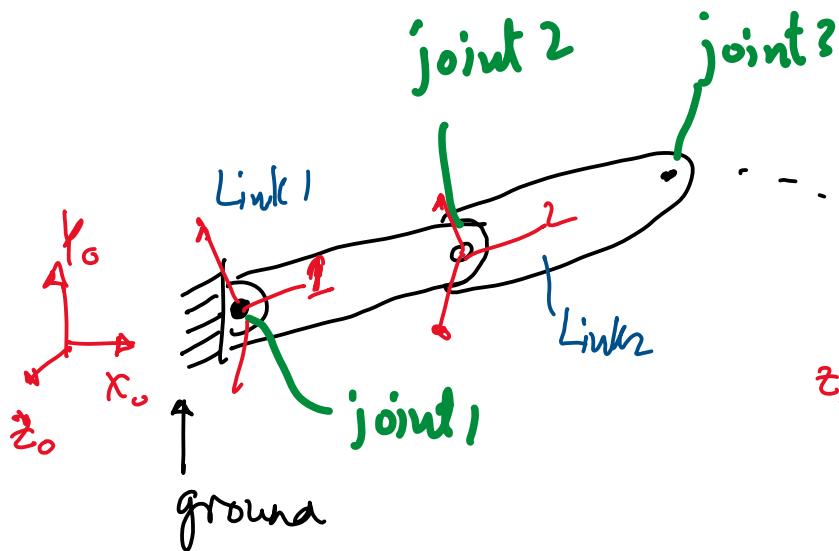
$$H_i^{i-1} = \begin{bmatrix} R_i^{i-1} & O_i^{i-1} \\ [0 \ 0]_{1 \times 2} & 1 \end{bmatrix}_{3 \times 3}$$

3D

$$H_i^{i-1} = \begin{bmatrix} R_i^{i-1} & O_i^{i-1} \\ [0 \ 0 \ 0]_{1 \times 3} & 1 \end{bmatrix}_{4 \times 4}$$



Kinematics



$$H_j^i = H_{i+1}^i H_{i+2}^{i+1} \cdots H_j^{j+1} \quad i < j$$

$$= I$$

$$= (H_i^j)^{-1}$$

$$i = j$$

$$i > j$$

$H \rightarrow 4 \times 4$ homogenous matrix.

$R_x(\phi)$

$$H_x(\phi) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos\phi & -\sin\phi \\ 0 & \sin\phi & \cos\phi \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \end{bmatrix}$$

no translation

4×4

$$H_y(\theta) = \begin{bmatrix} \cos\theta & 0 & \sin\theta & 0 \\ 0 & 1 & 0 & 0 \\ -\sin\theta & 0 & \cos\theta & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Revolute joint motion

$$H_z(\psi) = \begin{bmatrix} \cos\psi & -\sin\psi & 0 & 0 \\ \sin\psi & \cos\psi & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$H_x(a_x) = \begin{bmatrix} (1 & 0 & 0) & (q_x) \\ (0 & 1 & 0) & (0) \\ (0 & 0 & 1) & (0) \\ (0 & 0 & 0) & (1) \end{bmatrix}$$

$= I$ - translation

$$H_y(a_y) = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & a_y \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Prismatic joint motion

$$H_z(a_z) = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & a_z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Denavit-Hartenberg Convention (DH)

Method to represent the kinematics of a manipulator.

$$H_i^{i+1} = H_z(\underline{\alpha}_i) \underline{H}_z(d_i) H_x(a_i) H_x(\underline{\alpha}_i)$$

$$= \begin{bmatrix} \cos \underline{\alpha}_i & -\sin \underline{\alpha}_i & 0 & 0 \\ \sin \underline{\alpha}_i & \cos \underline{\alpha}_i & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & a_i \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos \underline{\alpha}_i & -\sin \underline{\alpha}_i & 0 \\ 0 & \sin \underline{\alpha}_i & \cos \underline{\alpha}_i & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\cos \underline{\alpha}_i = \cos \alpha_i$$

$$\cos \underline{\alpha}_i = \cos \alpha_i$$

$$\sin \underline{\alpha}_i = \sin \alpha_i$$

$$\sin \underline{\alpha}_i = \sin \alpha_i$$

To Represent 3D motion: 3 positions (x, y, z)
 ↓ 3 translation ($\theta_x, \theta_y, \theta_z$)
 we need 6 numbers

But DH convention uses only 4 numbers:
 $\underline{\alpha}_i, d_i, a_i, \underline{\alpha}_i$

This is possible because DH uses a special way to define the axis of the links

These 2 special things are:

① axis of $\underline{x_i}$ is perpendicular to $\underline{z_{i-1}}$

② axis of $\underline{x_i}$ intersects with $\underline{z_{i-1}}$

These 2 constraints help to get rid of 2 parameters. Hence DN uses only 4 parameters.

DH algorithm (1 of 2)

Algorithm for using DH for forward kinematics There are three steps.

1. Assign coordinate frames:

- (a) Assign z_i along the axis of actuation for each link, where $i = 0, 1, 2, \dots, (n - 1)$.
- (b) Assign the base frame $o_0 - x_0 - y_0 - z_0$. The z_0 has already been assigned. Assign x_0 arbitrarily. Assign y_0 based on x_0 and z_0 using right hand rule.
- (c) Now assign coordinate frames $o_i - x_i - y_i - z_i$ for $i = 1, 2, \dots, n - 1$. z_i is already attached in first step. Next we assign x_i using these rules.
 - i. z_{i-1} and z_i are not coplanar: In this case, there is a unique shortest distance segment that is perpendicular to z_{i-1} and z_i . Choose this as x_i axis. The origin o_i is where x_i intersects z_i . The y_i is found from right hand rule.
 - ii. z_{i-1} and z_i parallel: In this case, there infinitely many perpendiculars. Choose any of these perpendiculars for x_i . Furthermore, where x_i intersects z_i we draw the origin x_i . Finally, y_i is found from the right hand rule. To make equations simpler, choose x_i such that it passes through o_{i-1} . This will make $d_i = 0$. Also, since z_{i-1} is parallel to z_i , $\alpha_i = 0$.
 - iii. z_{i-1} and z_i intersect: In this case, x_i is chosen to be normal to the plane formed by z_{i-1} and z_i . There will be two possible directions for x_i , one of them is chosen arbitrarily and o_i is obtained by the intersection of z_{i-1} and x_i . Finally y_i is obtained from right hand rule. Also, since z_{i-1} intersects z_i , $a_i = 0$.
- (d) Finally we need to attach an end effector frame, $o_n - x_n - y_n - z_n$. Attach z_n to be the same direction as z_{n-1} . Now depending on the relation between z_n and z_{n-1} , attach frame x_n . Finally, attach y_n using the right hand rule.

DH algorithm (2 of 2)

2. Generate a table for DH parameter: Now generate the DH table as follows.

Link	a_i	α_i	d_i	θ_i
1				
2				
.				
.				
n				

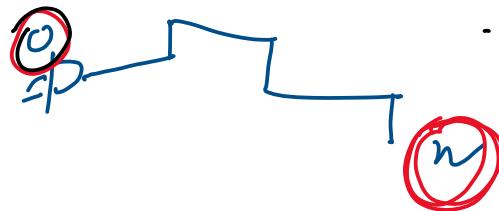
3. Apply DH transformation to evaluate forward kinematics: Finally, use the DH formulate to link two adjacent frames

$$H_i^{i-1} = \begin{bmatrix} c\theta_i & -s\theta_i c\alpha_i & s\theta_i s\alpha_i & a_i c\theta_i \\ s\theta_i & c\theta_i c\alpha_i & -c\theta_i s\alpha_i & a_i s\theta_i \\ 0 & s\alpha_i & c\alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

The position and orientation of the end-effector is found using the formula

$$H_n^0 = H_1^0 H_2^1 H_3^2 \dots H_{n-1}^{n-1} = [R_n^0 \quad d_n^0]$$

The position of the end-effector is d_n^0 and the orientation is R_n^0 . From R_n^0 , we can recover the Euler angles for the end-effector frame.

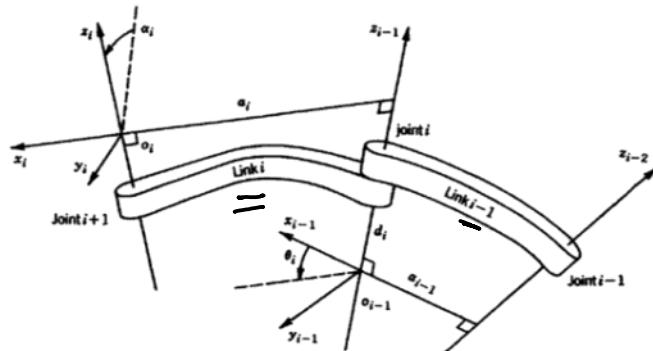


R_n^0 - orientation of
n-th axis
w.r.t. 0

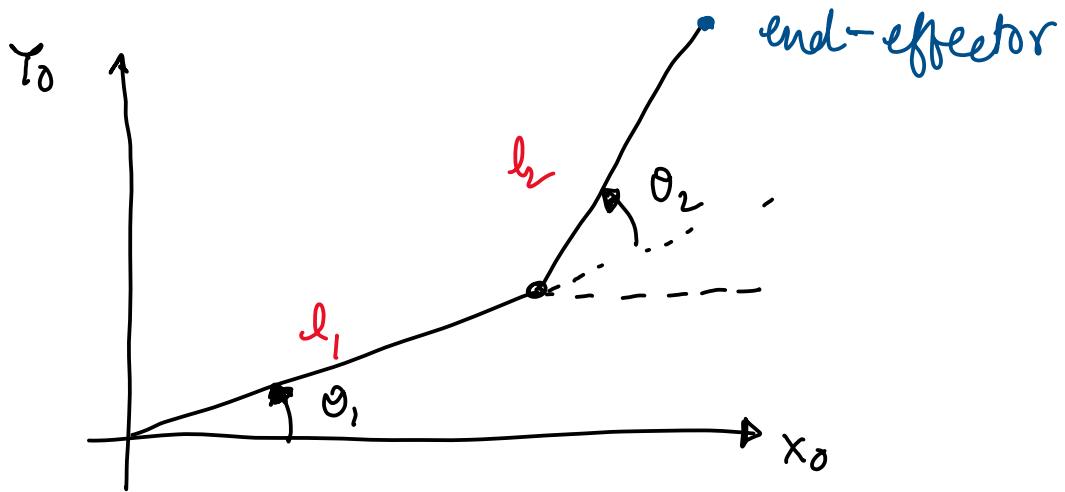
d_n^0 - position of
n-th axis
w.r.t. 0.

DH figure

1. a_i is the distance between z_i and z_{i-1} along x_i .
2. α_i is the angle between z_i and z_{i-1} along x_i .
3. d_i is the distance between x_{i-1} and x_i along z_{i-1} .
4. θ_i is the angle between x_{i-1} and x_i along z_{i-1} .

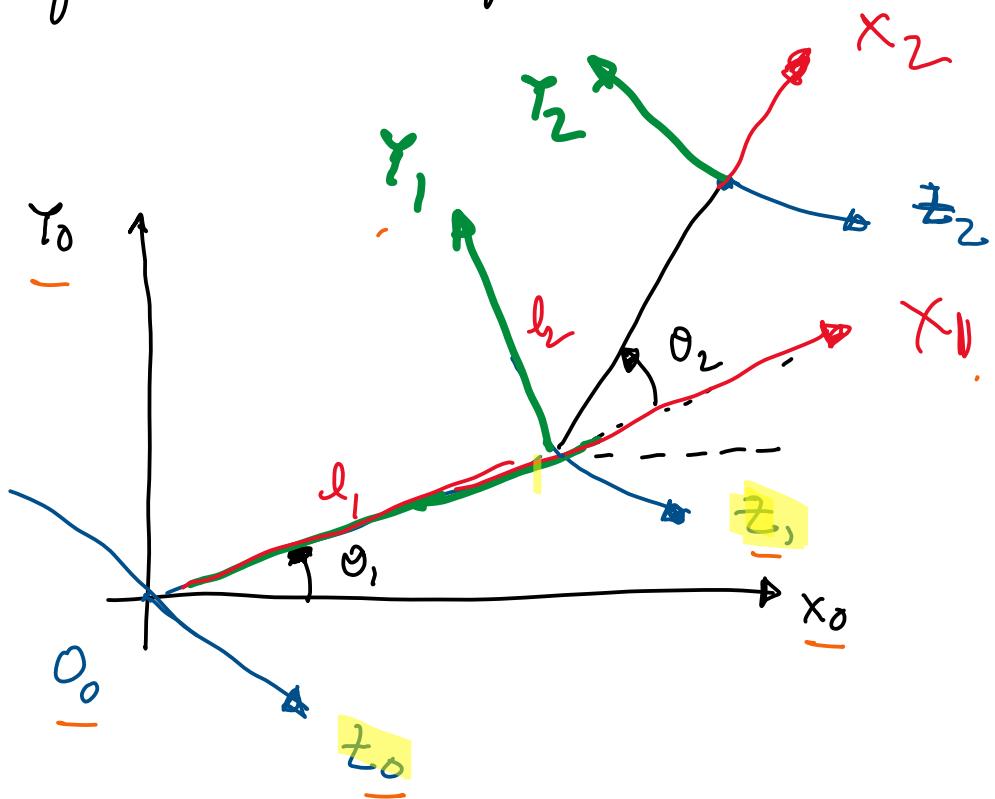


EXAMPLE 1

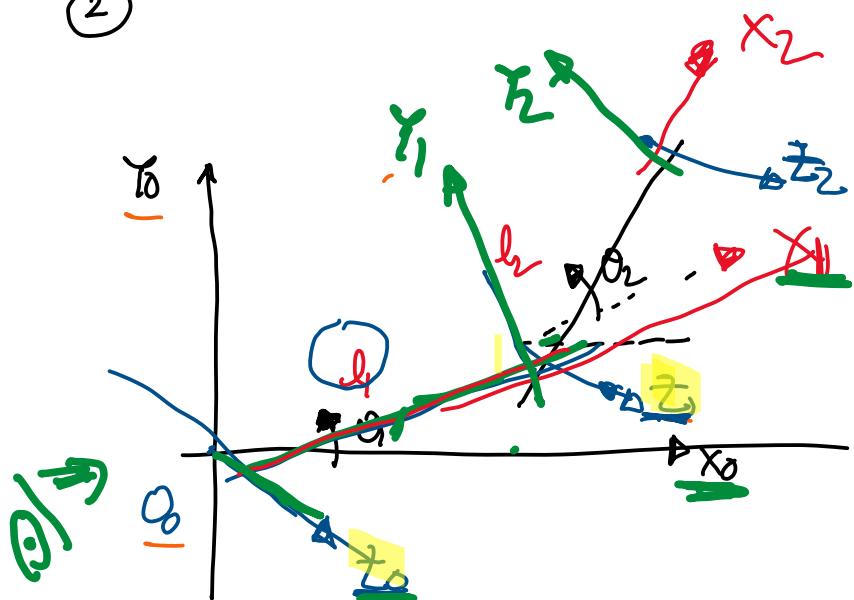


Compute the position and orientation of the end-effector

① Assign co-ordinate frames

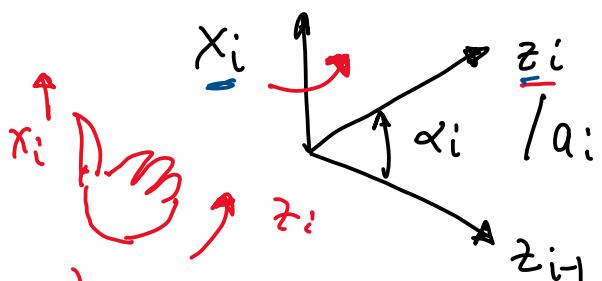


(2)



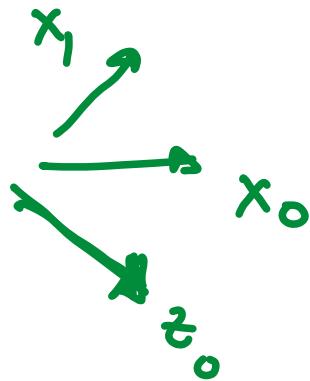
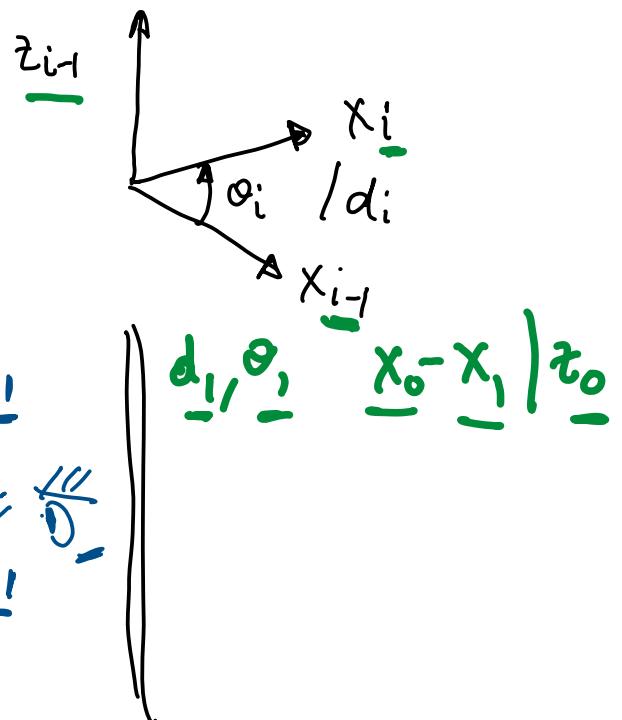
DH Table

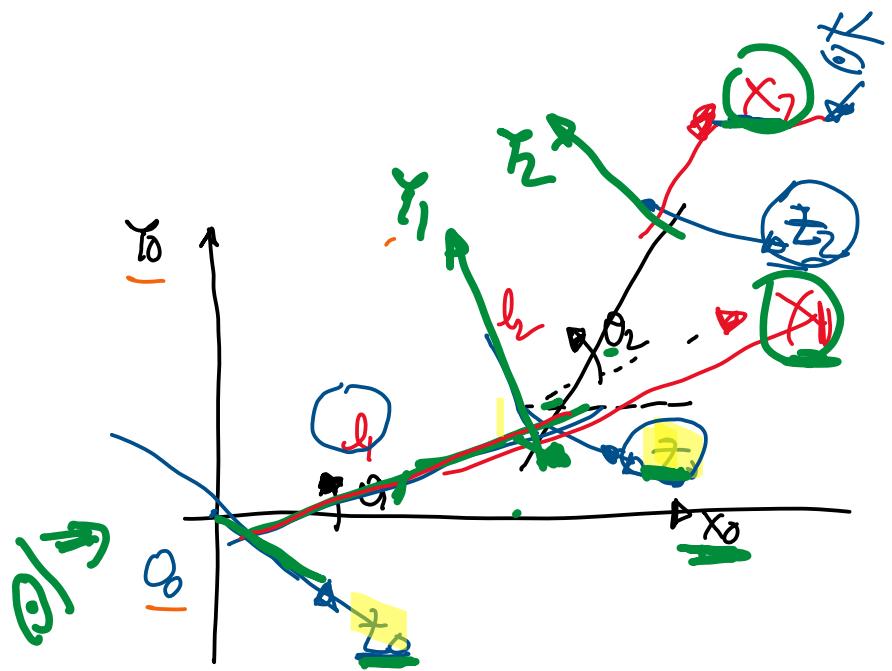
Link	a_i	α_i	d_i	θ_i
1	l_1	0	0	θ_1
2				



$$\underline{z}_0 - \underline{z}_1 \parallel \underline{x}_1$$

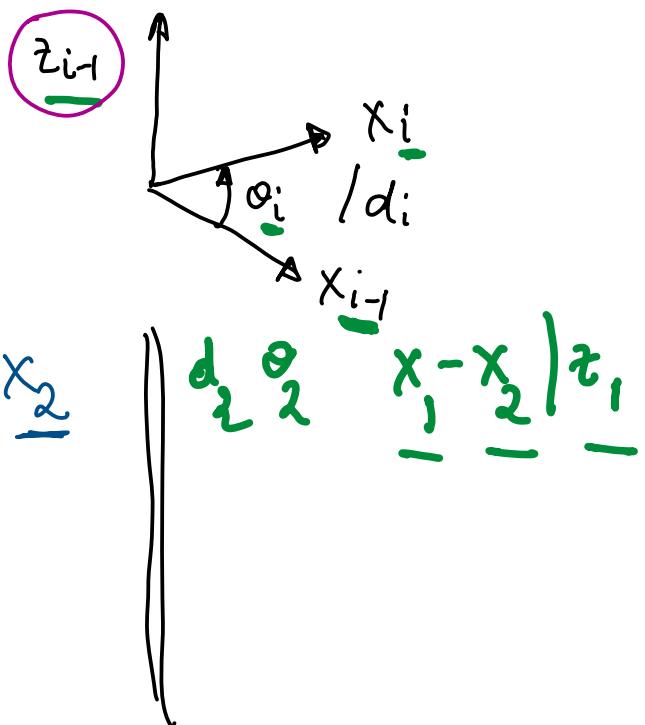
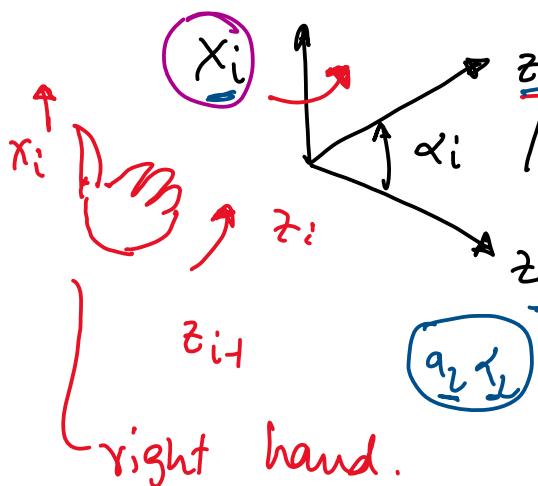
right hand.





DH Table

Link	a_i	α_i	d_i	θ_i
1	l_1	0	0	θ_1
2	l_2	0	0	θ_2



③ Use DH transformation

$$H_1^0 = \begin{bmatrix} c_1 & -s_1 & 0 & l_1 c_1 \\ s_1 & c_1 & 0 & l_1 s_1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad \begin{aligned} c_1 &= \cos \theta_1 \\ s_1 &= \sin \theta_1 \end{aligned}$$

From the first line of the DH table

Link 1	a_1	α_1	d_1	θ_1
	l_1	0	0	θ_1

$$H_2^1 = \begin{bmatrix} c_2 & -s_2 & 0 & l_2 c_2 \\ s_2 & c_2 & 0 & l_2 s_2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad \begin{aligned} c_2 &= \cos \theta_2 \\ s_2 &= \sin \theta_2 \end{aligned}$$

From the 2nd line of the DH table

Link 2	a_2	α_2	d_2	θ_2
	l_2	0	0	θ_2

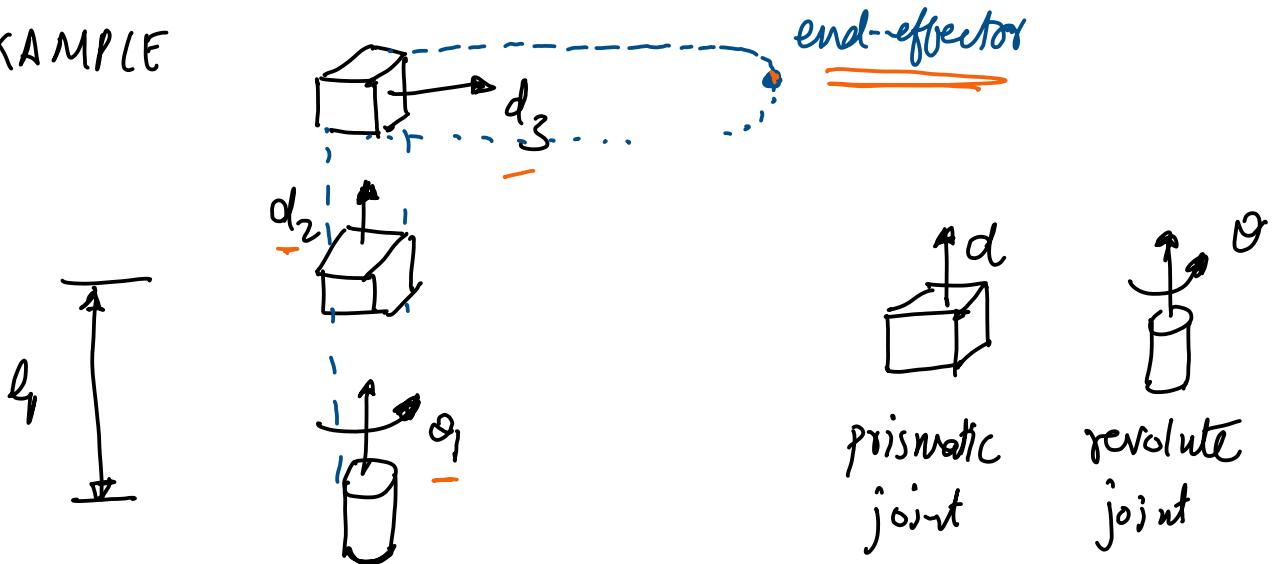
position of
the end-effector

$$H_2^0 = H_1^0 H_2^1 = \begin{bmatrix} c_2 & -s_2 & 0 \\ s_{12} & c_{12} & 0 \\ 0 & 0 & 1 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} l_1 c_1 + l_2 c_2 \\ l_1 s_1 + l_2 s_{12} \\ 0 \\ 1 \end{bmatrix}$$

$$c_2 = \cos(\theta_1 + \theta_2); \quad s_{12} = \sin(\theta_1 + \theta_2)$$

orientation of
the end-effector

(2) EXAMPLE



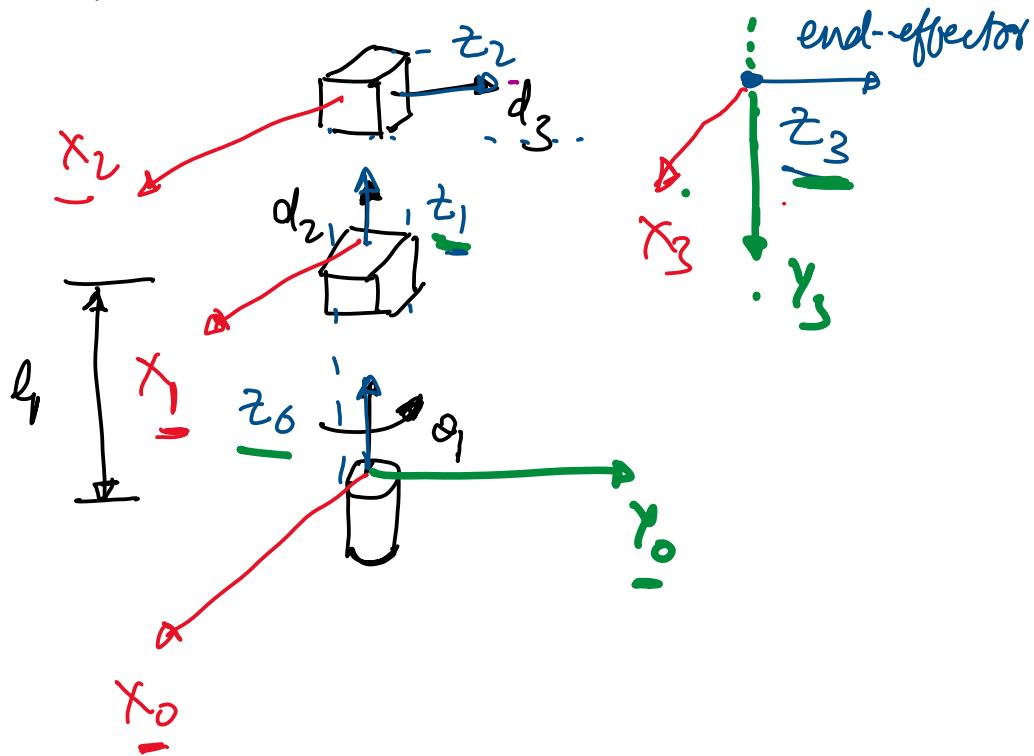
- ✓ 1 Revolute (1R)
- ✓ 2 prismatic (2P)

Links are NOT shown
Only the joints are shown.

1R - 2P manipulator

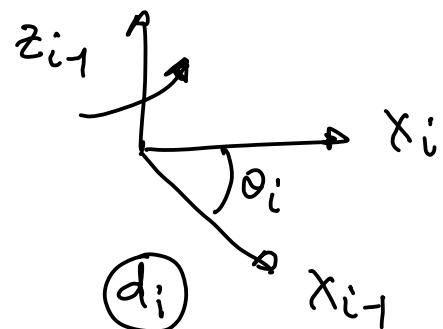
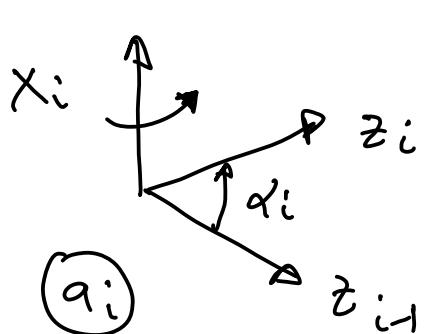
Compute the position and orientation of the end-effector using DH convention

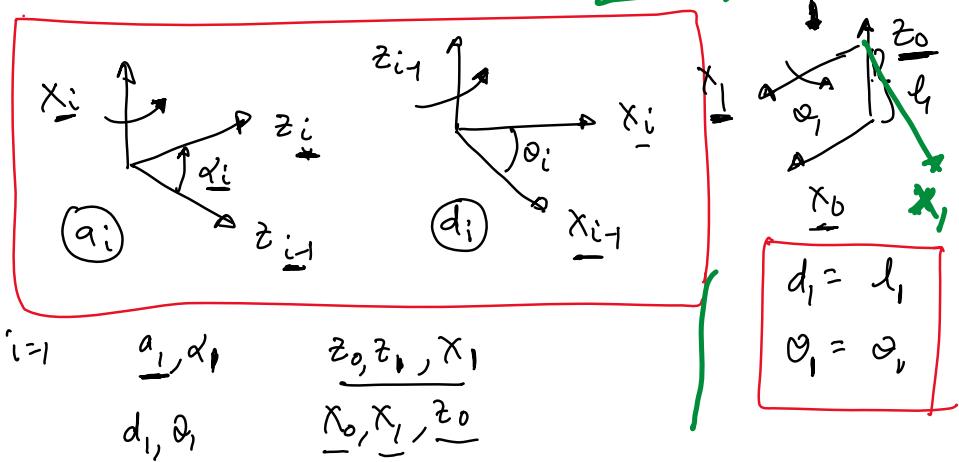
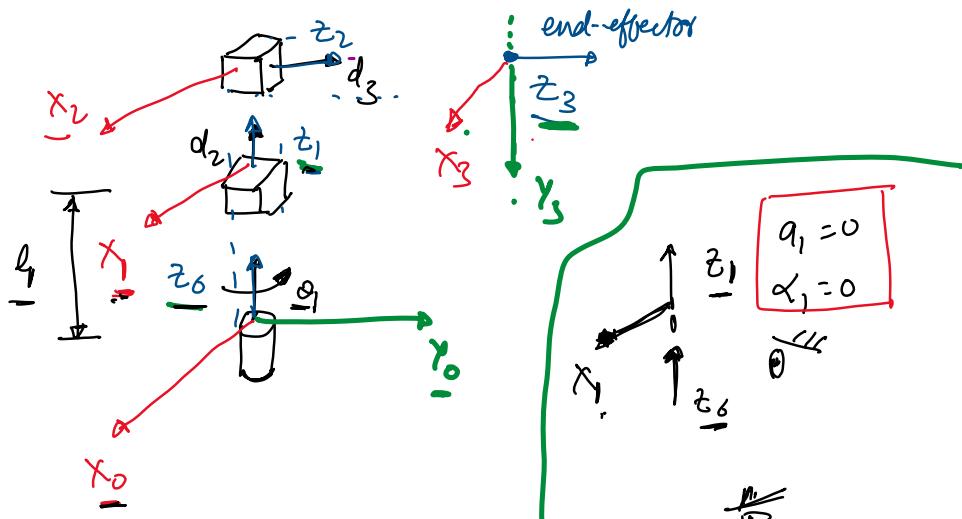
① Assign co-ordinate frames

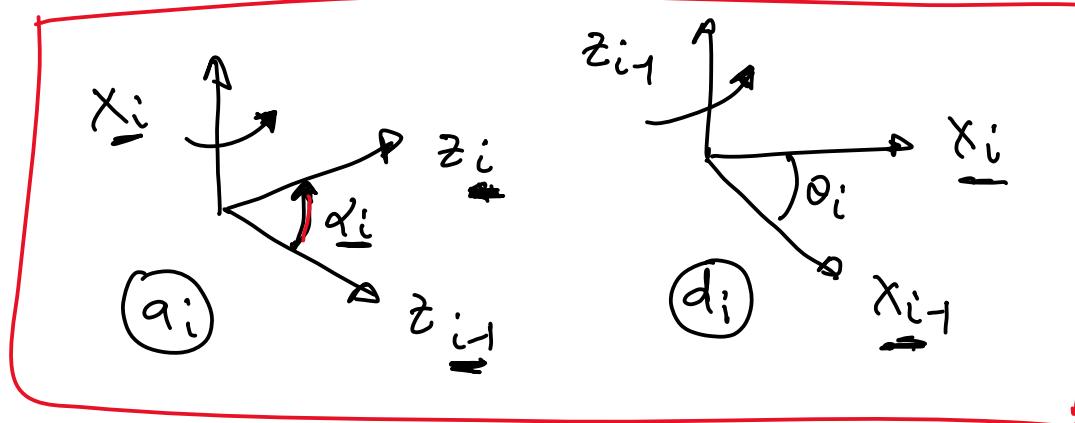
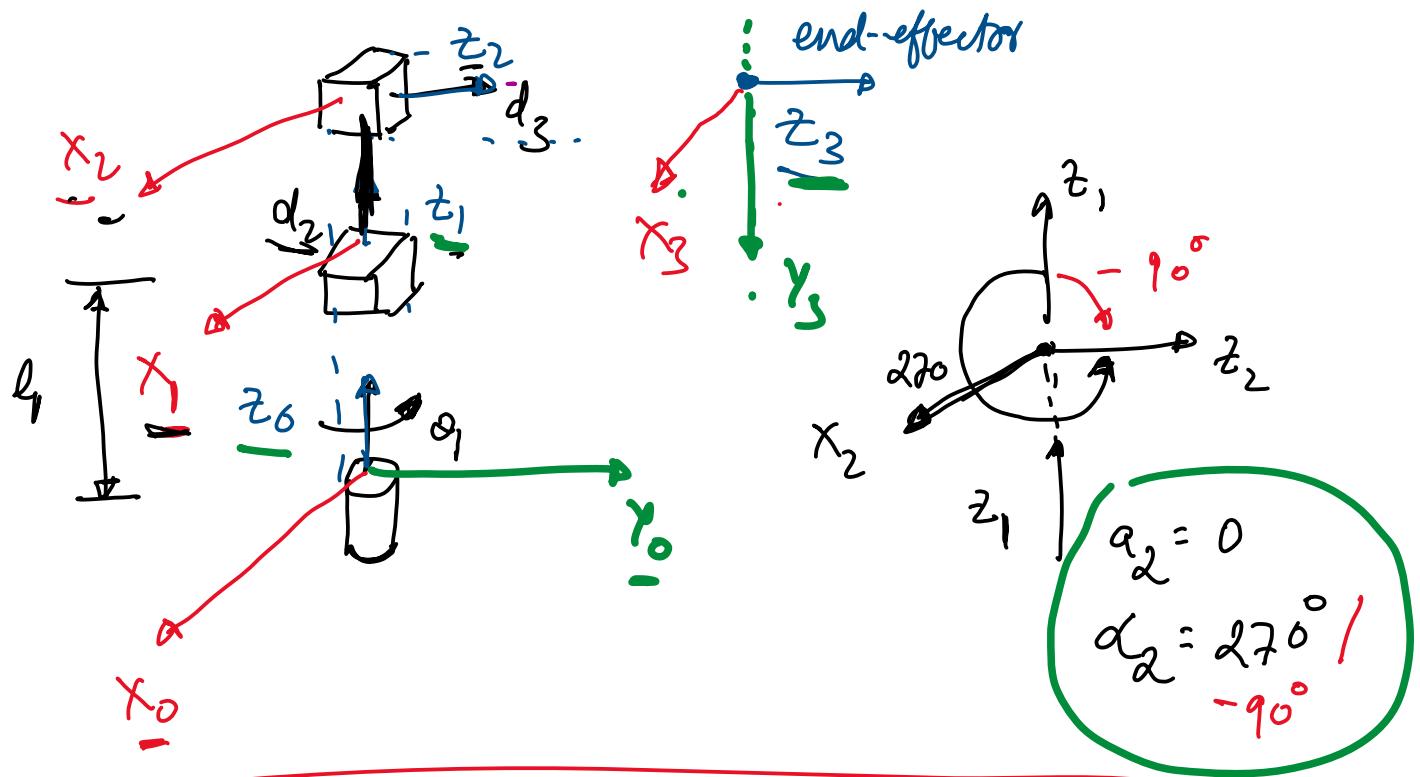


② DH table

Link	a_i	α_i	d_i	θ_i
1	0	0	l_1	q_1
2	0	$270^\circ - q_0$	d_2	0
3	0	0	d_3	0



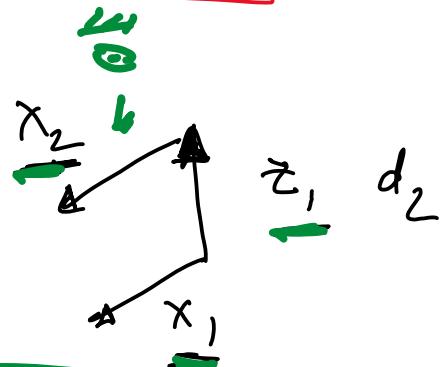




$i=2$

$$\underline{z_1}, \underline{z_2}, x_2$$

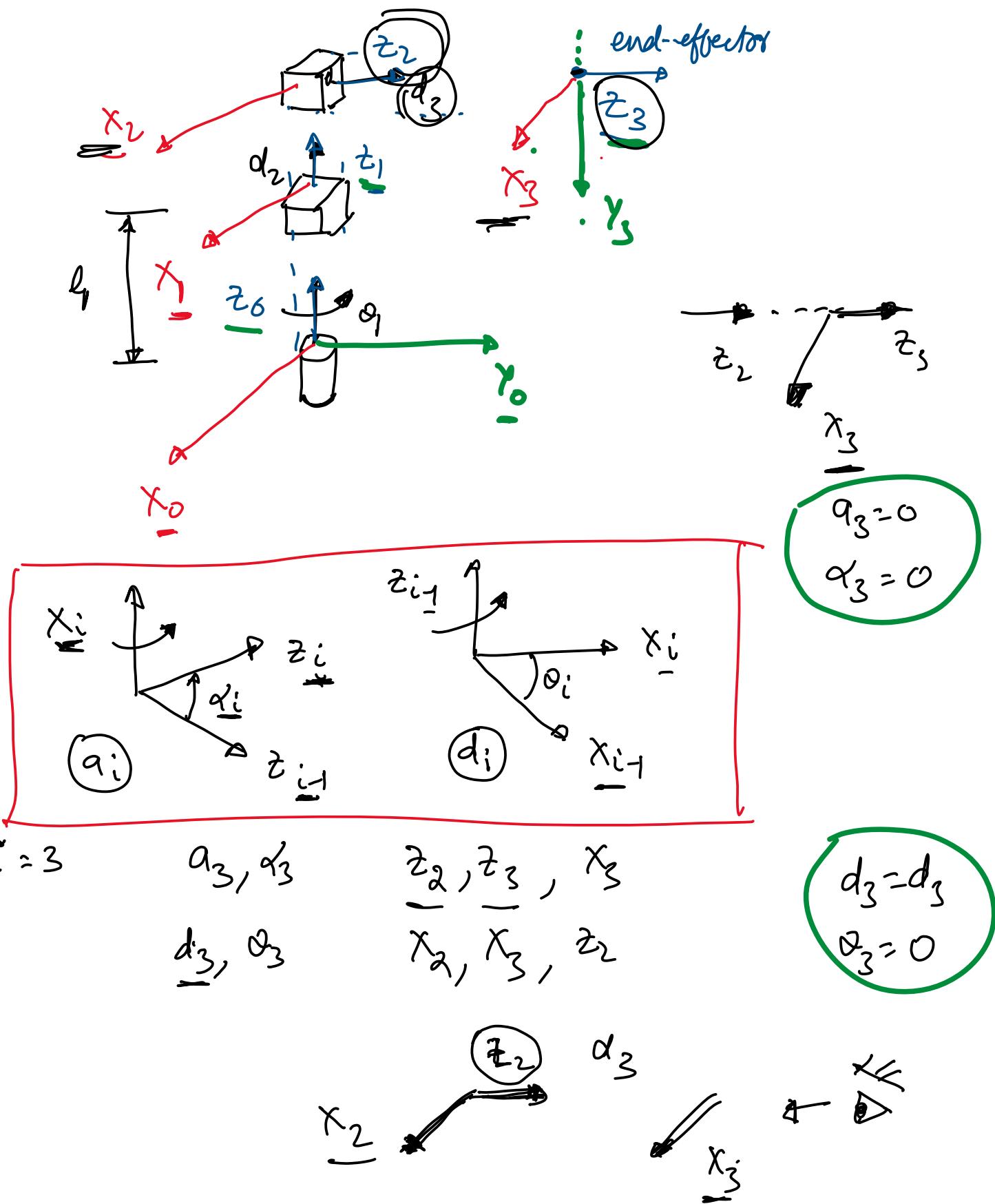
$$x_1, x_2, \underline{z_1}$$



$$d_2 = d_2$$

$$d_2 = \alpha_2$$

$$\theta_2 = 0$$



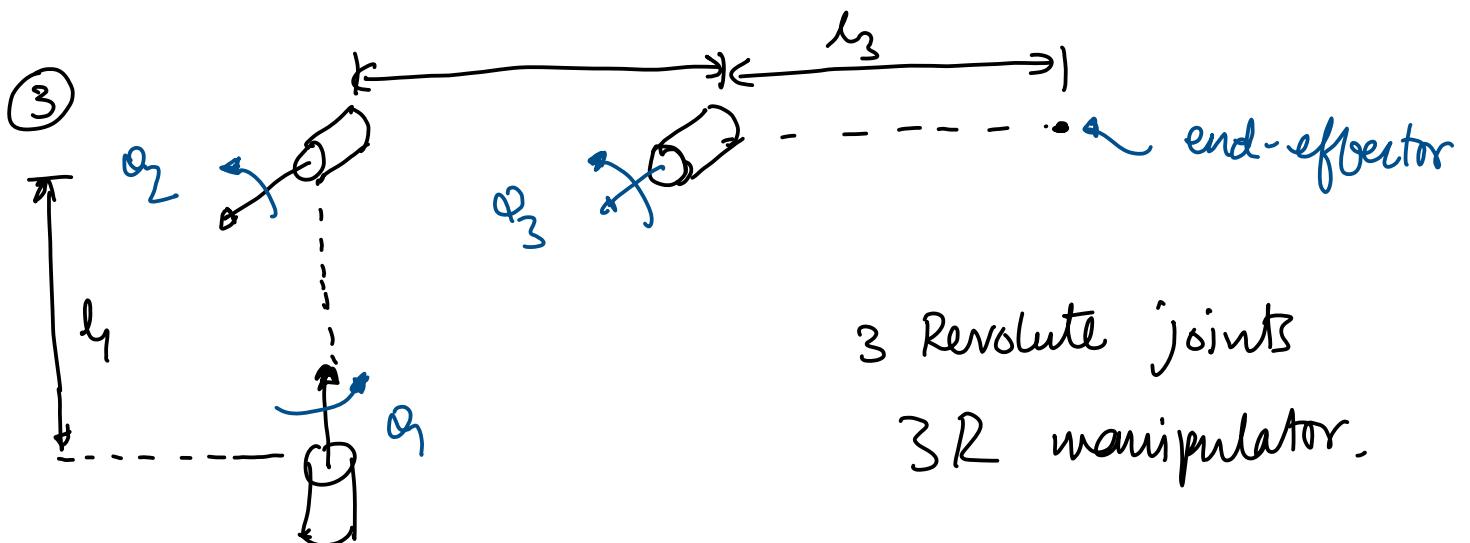
③ Compute H_i^{i+1} using the D-H formula.

$$H_1^0, H_2^1, H_3^2 \quad \checkmark$$

$$H_3^0 = H_1^0 H_2^1 H_3^2 = \begin{bmatrix} (R_3^0) & (d_3^0) \\ 0 & 1 \end{bmatrix}$$

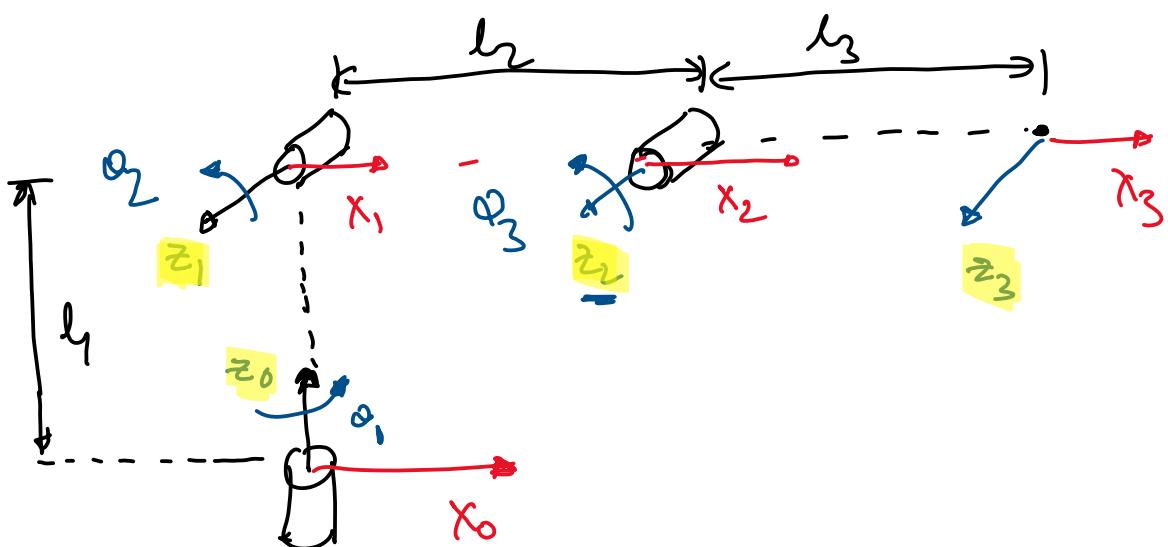
position of
 the
 end-effector

orientation of
 the end-effector

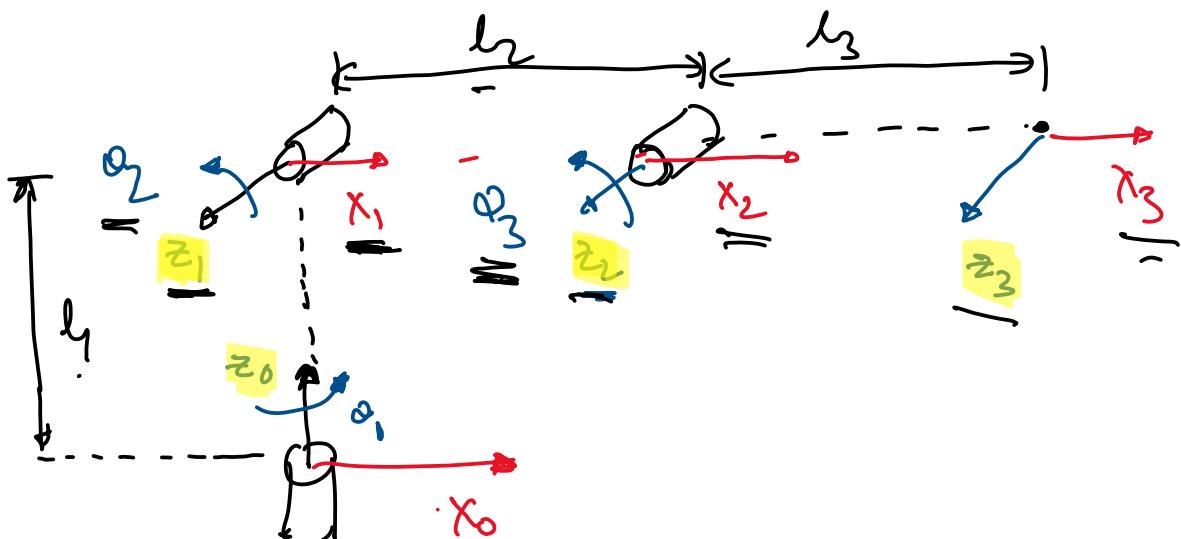


Compute the position and orientation of the end-effector

①

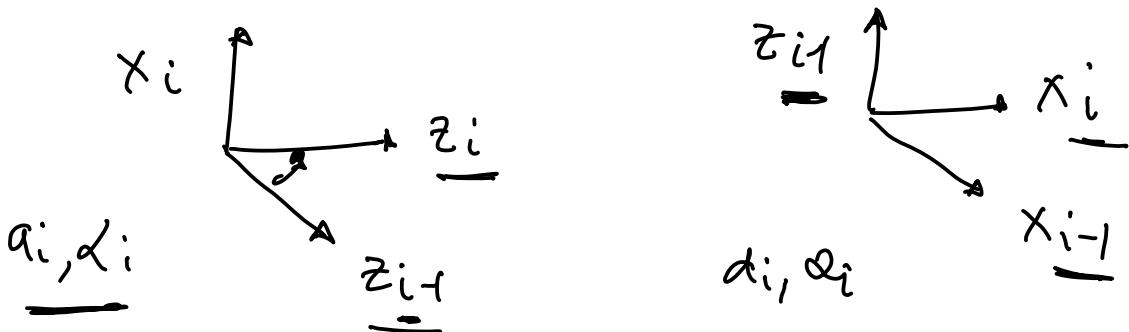


$$x_1 \perp z_0, z_1$$



(2)

Link	a_i	α_i	d_i	θ_i	
1	0	90°	l_1	θ_1	1
2	l_2	0	0	θ_2	2
3	l_3	0	0	θ_3	3



$$\textcircled{3} \quad H_i^{i-1} = \begin{bmatrix} & & & \\ & & & \\ & & & \\ & & & \end{bmatrix}_{4 \times 4}$$

$$i=1 \quad H_1^0 = []_{4 \times 4}$$

$$i=2 \quad H_2^1 = []_{4 \times 4}$$

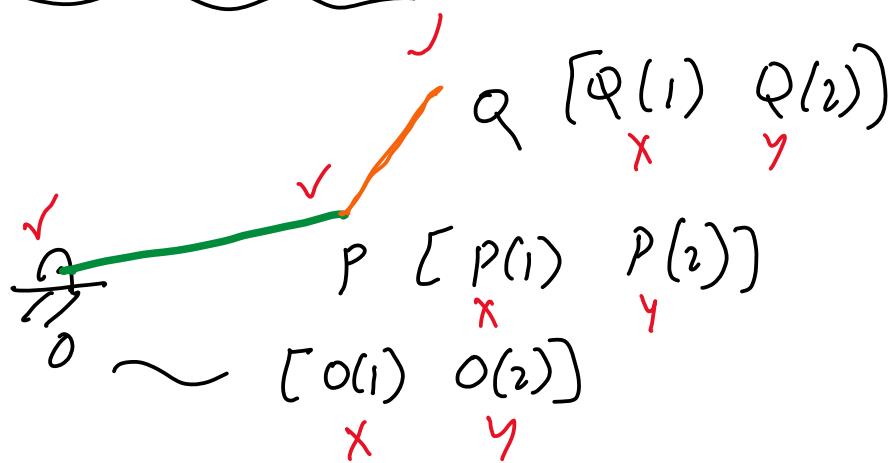
$$i=3 \quad H_3^2 = []_{4 \times 4}$$

$$H_3^0 = H_1^0 H_2^1 H_3^2 = \begin{bmatrix} R_3^0 & O_3^0 \\ 0 & 1 \end{bmatrix}$$

3x3
 position
 3x3
 orientation

Animation / Visualization

2D



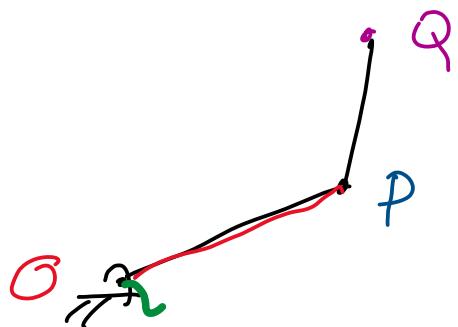
we compute $(O[1], O[2]), (P[1], P[2]),$
 $[Q(1), Q(2)]$

using homogeneous transformation in 2D

line $(\underbrace{O(1)}_x \underbrace{P(1)}_y), (\underbrace{O(2)}_x \underbrace{P(2)}_y)$

line $([P(1), Q(1)], [P(2), Q(2)])$

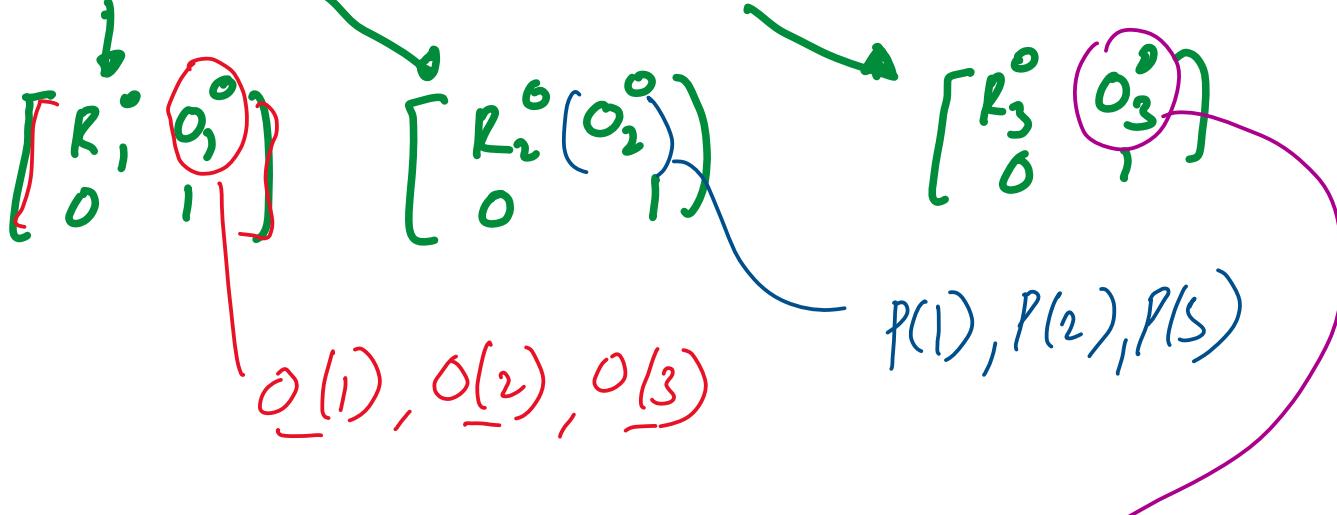
3D



$$H_1^0, H_2^1, H_3^2$$

✓

$$H_1^0, H_2^0 = H_1^0 H_2^1, H_3^0 = H_1^0 H_2^1 H_3^2$$



line $\left(\underbrace{(\alpha_1)}_x P(1), \underbrace{(\alpha_2)}_y P(2), \underbrace{(\alpha_3)}_z P(3) \right)$

line $\left((P(1), Q(1)), \underbrace{(P(2), Q(2))}_x, \underbrace{(P(3), Q(3))}_z \right)$