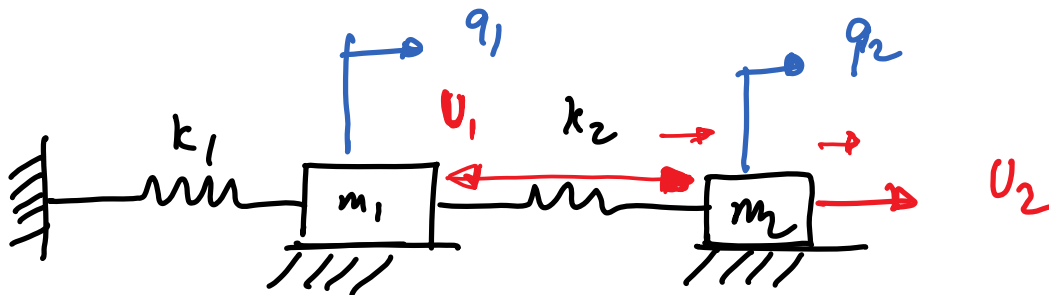


# Linear Control

System is linear in state (control)



$m_1, m_2$  — masses

$k_1, k_2$  — spring constant

$u_1, u_2$  — controls (forces)

$q_1, q_2$  — mass displacements

$$T = 0.5 m_1 \dot{q}_1^2 + 0.5 m_2 \dot{q}_2^2$$

$$V = 0.5 k_1 q_1^2 + 0.5 k_2 (q_1 - q_2)^2$$

$$\mathcal{L} = T - V$$

$$\mathcal{L} = 0.5 m_1 \dot{q}_1^2 + 0.5 m_2 \dot{q}_2^2 + 0.5 k_1 q_1^2 + 0.5 k_2 (q_1 - q_2)^2$$

$$\mathcal{L} = 0.5 \underline{m_1} \dot{q}_1^2 + 0.5 m_2 \dot{q}_2^2 + 0.5 k_1 q_1^2 + 0.5 k_2 (q_1 - q_2)^2$$

$$\frac{d}{dt} \left( \frac{\partial \mathcal{L}}{\partial \dot{q}_j} \right) - \frac{\partial \mathcal{L}}{\partial q_j} = Q_j \quad j=1,2$$

$$\textcircled{1} \quad q_1: \frac{d}{dt} (0.5 (2m_1 \dot{q}_1)) + 0.5 (2k_1 q_1) + 0.5 (2k_2)(q_1 - q_2) = -u_1$$

$$m_1 \ddot{q}_1 + k_1 q_1 + k_2 (q_1 - q_2) = -u_1$$

$$\ddot{q}_1 = - \left( \frac{k_1}{m_1} + \frac{k_2}{m_1} \right) q_1 + \frac{k_2}{m_1} q_2 - \frac{u_1}{m_1} \quad \textcircled{1}$$

$$\textcircled{2} \quad q_2: \frac{d}{dt} (0.5 (2m_2 \dot{q}_2)) + 0.5 (2k_1)(q_1 - q_2) (-1) = u_1 + u_2$$

$$m_2 \ddot{q}_2 + k_1 (q_2 - q_1) = u_1 + u_2$$

$$\ddot{q}_2 = \frac{k_2}{m_2} q_1 - \frac{k_2}{m_2} q_2 + \frac{U_1}{m_2} + \frac{U_2}{m_2} \quad \text{--- (2)}$$

State space representation

$$x_1 = q_1$$

$$x_2 = q_2$$

$$x_3 = \dot{q}_1$$

$$x_4 = \dot{q}_2$$

$$\rightarrow \dot{x}_1 = \dot{q}_1 = x_3$$

$$\dot{x}_2 = \dot{q}_2 = x_4 \quad \text{--- from (1)}$$

$$\dot{x}_3 = \ddot{q}_1 = -\left(\frac{k_1}{m_1} + \frac{k_2}{m_1}\right)x_1 + \left(\frac{k_2}{m_1}\right)x_2 - \frac{U_1}{m_1}$$

$$\dot{x}_4 = \ddot{q}_2 = \frac{k_2}{m_2} x_1 - \frac{k_2}{m_2} x_2 + \frac{U_1}{m_1} + \frac{U_2}{m_2}$$

--- from (2)

$$X = [x_1, x_2, x_3, x_4]$$

$$\dot{X} = AX + BU$$

$$4 \times 1 \quad 4 \times 4 \quad 4 \times 1 \quad 4 \times 2 \quad 2 \times 1$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \\ \dot{x}_4 \end{bmatrix} = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ -\left(\frac{k_1}{m_1} + \frac{k_2}{m_1}\right) & \frac{k_2}{m_1} & 0 & 0 \\ \frac{k_2}{m_2} & \frac{k_2}{m_2} & 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ x_4 \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ \frac{1}{m_1} & 0 \\ \frac{1}{m_2} & \frac{1}{m_2} \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}$$

$4 \times 4$ 
 $4 \times 2$

state-space equation

Check stability of uncontrolled system

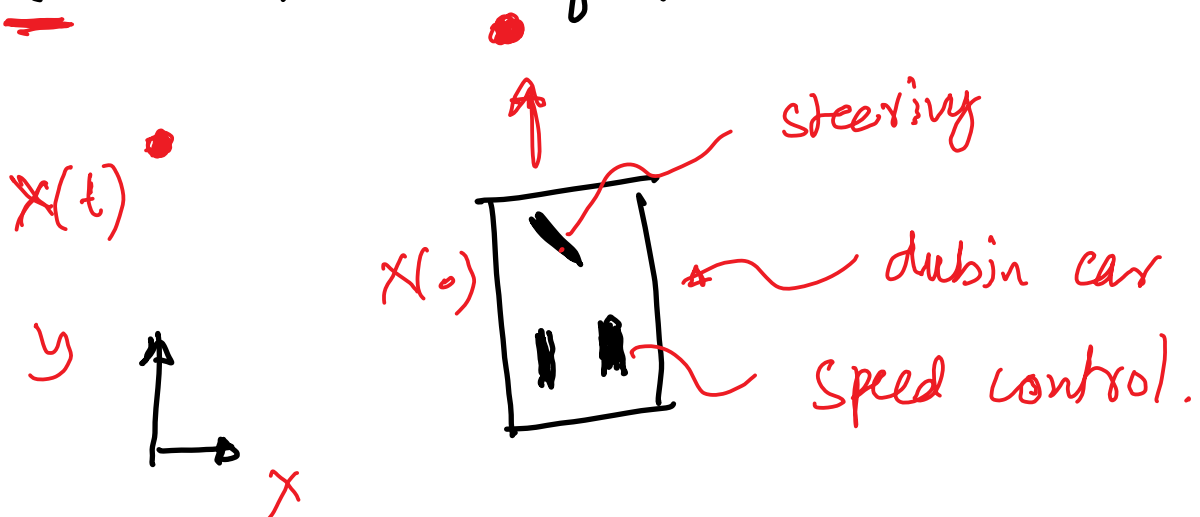
$$\dot{X} = AX \quad \text{— uncontrolled system}$$

Compute eigenvalues and check if all the real parts are negative. If they are negative then the system is stable

Use control ( $u$ ) to either stabilize the system or make it more stable

However, one needs to check if the system is controllable

Controllability: A linear system is controllable if and only if it can be transferred from any initial state  $x(0)$  to any terminal state  $x(t)$  within a finite time



$$\Rightarrow C_0 = [A^{n-1}B, A^{n-2}B, A^{n-3}B, \dots, AB, B]$$

$n$  = system dof e.g. spring-mass  $n=4$

$\Rightarrow$  rank  $(C_0) = n$  system is controllable  
rank  $(C_0) < n$  system is not controllable

pip install control

import control

$C_0 = \text{control.ctrb}(A, B)$

np.linalg.matrix\_rank( $C_0$ )

## Methods of control

### ① Pole placement

Assume  $u = -Kx$        $K = \text{gain matrix}$

$$\dot{x} = Ax + Bu$$

$$= Ax - BKx$$

$$\dot{x} = \underbrace{(A - BK)}_x x$$

place eigenvalues at a certain  
place poles at "p" ← location  
↑ user choice

$K = \text{control. place}(A, B, p)$   
↑ user choice

### ② Linear quadratic controller

## ② Linear quadratic controller

$$\rightarrow \dot{x} = Ax + Bu$$

compute  $u$  such that it minimizes

$$J = \overbrace{x^T(t_f) F x(t_f)} - \text{terminal cost} + \dots + \int_0^{t_f} (x^T Q x + \underline{\underline{u^T R u}} + 2x^T N u) dt$$

$F, Q, R, N$  — user chosen matrices

$Q \gg R$  aggressive control

$Q \ll R$  less aggressive control

$Q >$  positive definite — eigenval  $> 0$

$R \geq$  semi-positive definite — eigenval  $\geq 0$

---

$$u = -Kx$$

$\uparrow$  gain  $K$



?

$$K = R^{-1} (B^T P + N^T) \quad \{ U = -Kx \}$$

$$-\dot{P} = A^T P + PA - (PB + N) R^{-1} (B^T P + N^T) + Q = 0$$

Ricatti differential equation

$$P(t_f) = F(t_f)$$

Special case

$$J = \int_0^{\infty} (x^T Q x + u^T R u + 2 x^T N u) dt$$

infinite horizon problem

$$U = -Kx \quad \& \quad K = -R^{-1} (B^T P + N^T)$$

$$AP + PA - (PB + N) R^{-1} (B^T P + N^T) + Q = 0$$

steady state Ricatti equation

$$K, P, E = \text{control. } 1 \times n (A, B, Q, R, N)$$

gain

Solution to Ricatti equation

eigenvalues of closed loop:  $\text{eig}(A - BK)$

# Linear control for a non-linear system

$$\dot{x} = F(x, u) \quad \text{--- (1)}$$

we will linearize this system about an operating point  $(x_0, u_0)$  and use the linearized system for control,

$$x \rightarrow x_0 + \delta x \quad ; \quad u \rightarrow u_0 + \delta u$$

Putting this in (1)

$$\dot{x}_0 + \delta \dot{x} = F(x_0 + \delta x, u_0 + \delta u)$$

Taylor series.  
↗

$$\dot{x}_0 + \delta \dot{x} = F(x_0, u_0) + \frac{\partial F}{\partial x} (x - x_0) + \frac{\partial F}{\partial u} (u - u_0)$$

$$\dot{x}_0 = F(x_0, u_0)$$

+ higher order terms

$$\delta \dot{x} = \frac{\partial F}{\partial x} \delta x + \frac{\partial F}{\partial u} \delta u$$

$$\delta \dot{x} = \frac{\partial f}{\partial x} \delta x + \frac{\partial f}{\partial u} \delta u$$

$$\delta \dot{x} = A \delta x + B \delta u$$

$$\text{where } A = \frac{\partial f}{\partial x} ; B = \frac{\partial f}{\partial u}$$

① use lqr / pole placement to compute

$$\delta u = -K \delta x$$

② Note the control is

$$u = u_0 + \delta u$$

Example:

Differential drive car

$$\dot{x} = v \cos \theta$$

$$\dot{y} = v \sin \theta$$

$$\dot{\theta} = \omega$$

$$X = [x, y, \theta]^T ; u = [v, \omega]$$

Assume an operating point  $x_0, u_0$

Assume an operating point  $\lambda_0, u_0 \rightarrow (x_0, y_0, \theta_0)$   $(v_0, w_0)$

$$\delta \ddot{x} = A \delta x + B \delta u$$

$$f = \begin{bmatrix} v \cos \alpha \\ v \sin \alpha \\ w \end{bmatrix} \quad X = \begin{bmatrix} x \\ y \\ \alpha \end{bmatrix} \quad \bar{B}(\alpha) \begin{bmatrix} v \\ w \end{bmatrix}$$

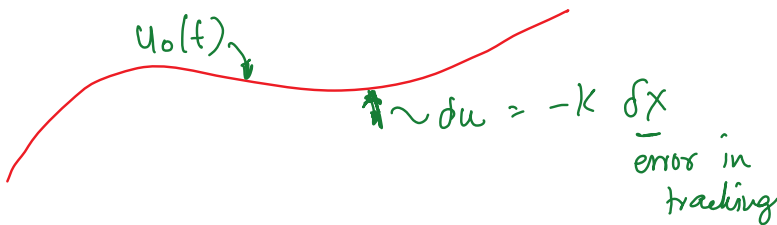
$$A = \frac{\partial f}{\partial x} = \begin{bmatrix} \frac{\partial (v \cos \alpha)}{\partial x} & \frac{\partial (v \cos \alpha)}{\partial y} & \frac{\partial (v \cos \alpha)}{\partial \alpha} \\ \frac{\partial (v \sin \alpha)}{\partial x} & \frac{\partial (v \sin \alpha)}{\partial y} & \frac{\partial (v \sin \alpha)}{\partial \alpha} \\ \frac{\partial w}{\partial x} & \frac{\partial w}{\partial y} & \frac{\partial w}{\partial \alpha} \end{bmatrix}$$

$$= \begin{bmatrix} 0 & 0 & -v \sin \alpha \\ 0 & 0 & v \cos \alpha \\ 0 & 0 & 0 \end{bmatrix}$$

$$B = \frac{\partial F}{\partial u} = \begin{matrix} \begin{matrix} \frac{\partial v \cos \alpha}{\partial v} & \frac{\partial v \cos \alpha}{\partial \omega} \\ \frac{\partial v \sin \alpha}{\partial v} & \frac{\partial v \sin \alpha}{\partial \omega} \\ \frac{\partial \omega}{\partial v} & \frac{\partial \omega}{\partial \omega} \end{matrix} \\ \downarrow \\ (v, \omega) \end{matrix} = \begin{bmatrix} \cos \alpha & 0 \\ \sin \alpha & 0 \\ 0 & 1 \end{bmatrix}$$

$$\delta \dot{x} = \begin{bmatrix} 0 & 0 & -v_0 \sin \alpha_0 \\ 0 & 0 & v_0 \cos \alpha_0 \\ 0 & 0 & 0 \end{bmatrix} \delta x + \begin{bmatrix} \cos \alpha_0 & 0 \\ \sin \alpha_0 & 0 \\ 0 & 1 \end{bmatrix} \delta u$$

$u = u_0 + \delta u$  → pole placement / LQR (feedback)  
 ↘ found using trajectory optimization (open-loop)



This controller is different from what we did previously

$$\dot{x} = f(x, u) \quad \text{— car}$$

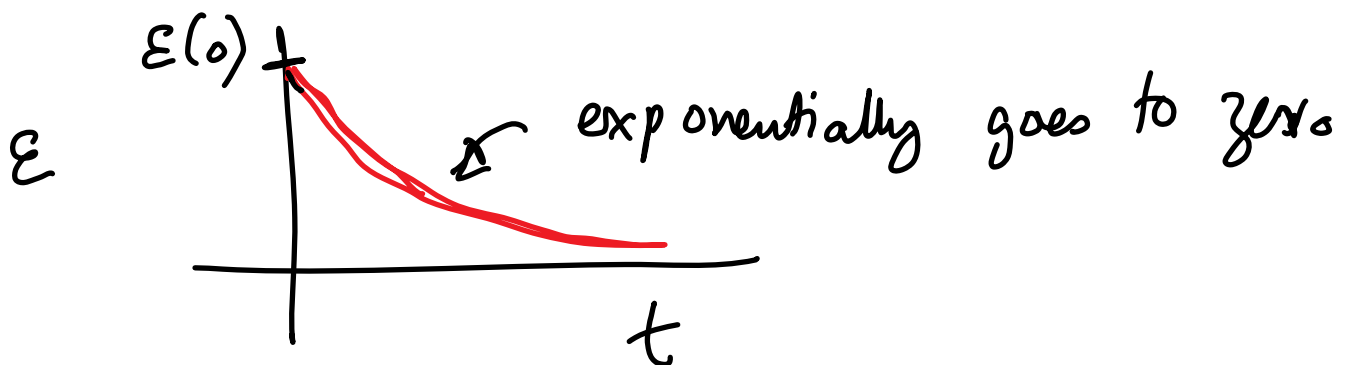
$$\dot{x} = \dot{x}_{\text{ref}} + k_p (x_{\text{ref}} - x) \quad \text{— controller for car}$$

[feedback  
linearization]

$$\underbrace{\dot{x} - \dot{x}_{\text{ref}}}_{\dot{\varepsilon}} = k_p \underbrace{(x_{\text{ref}} - x)}_{-\varepsilon}$$

$$\underline{\underline{\dot{\varepsilon} + k_p \varepsilon = 0}}$$

$$\Rightarrow \boxed{\varepsilon = A e^{-k_p t}}$$



# Manipulator system

$$M(q) \ddot{q} + C(q, \dot{q}) \dot{q} + G(q) = \overline{B}(q) u$$

$\overline{B}(q) u$  —  $m \times 1$   
 $\swarrow$   
 $n \times m$

$$\dot{x} = F(x, u)$$

$$x = \begin{bmatrix} q \\ \dot{q} \end{bmatrix} \begin{array}{l} \text{— angle} \\ \text{— angular velocity.} \end{array}$$

$$\begin{aligned} \dot{x} = \begin{bmatrix} \dot{q} \\ \ddot{q} \end{bmatrix} &= \begin{bmatrix} \dot{q} \\ M^{-1}(q) \{ -G(q) - C(q, \dot{q}) \dot{q} + \overline{B}(q) u \} \end{bmatrix} \\ &= F(x, u) \end{aligned}$$

$$\dot{x} = F(x, u) = \begin{bmatrix} f_1 \\ f_2 \end{bmatrix}$$



$$\tilde{A} = \frac{\partial f}{\partial x} \quad ; \quad \tilde{B} = \frac{\partial f}{\partial u}$$

$$f = \begin{bmatrix} f_1 \\ f_2 \end{bmatrix} = \begin{bmatrix} \dot{q} \\ M^{-1}(q) \{ -L(q, \dot{q})\dot{q} - G(q) + B(q)u \} \end{bmatrix}$$

$$x = [q, \dot{q}]$$

$$\hat{A} = \frac{\partial f}{\partial x} = \begin{bmatrix} \frac{\partial f_1}{\partial q} & \frac{\partial f_1}{\partial \dot{q}} \\ \frac{\partial f_2}{\partial q} & \frac{\partial f_2}{\partial \dot{q}} \end{bmatrix}$$

$$= \begin{bmatrix} \cancel{\frac{\partial \dot{q}}{\partial q}} & \frac{\partial \dot{q}}{\partial \dot{q}} \\ \frac{\partial f_2}{\partial q} & \frac{\partial f_2}{\partial \dot{q}} \end{bmatrix} \approx I$$

$$\frac{\partial f_2}{\partial q} = \frac{\partial}{\partial q} M^T(q) [-C(q, \dot{q})\dot{q} - G(q) + B(q)u]$$

$M \ddot{q} \approx 0$  at the operating point

$$= \frac{\partial M^T(q)}{\partial q} [-C(q, \dot{q})\dot{q} - G(q) + B(q)u]$$

$$+ M^T(q) \left[ - \frac{\partial C(q, \dot{q})\dot{q}}{\partial q} - \frac{\partial G}{\partial q} + \frac{\partial B(q)u}{\partial q} \right]$$

$=$

$\neq 0$

$\dot{q} = 0$  at the operating point

Trick:  $MM^T = I$

$$\frac{\partial M}{\partial q} M^T + M \frac{\partial M^T}{\partial q} = 0$$

$$M \frac{\partial M^T}{\partial q} = - \frac{\partial M}{\partial q} M^T$$

Pre-multiply with  $M^T$

$$\underbrace{M^T M}_I \frac{\partial M^T}{\partial q} = - M^T \frac{\partial M}{\partial q} M^T$$

$$\frac{\partial M^T}{\partial q} = - M^T \left( \frac{\partial M}{\partial q} \right) M^T$$

$$\frac{\partial f_2}{\partial q} = -M^T(q) \frac{\partial G}{\partial q} + \sum_j M^T \frac{\partial B_j}{\partial q} u_j$$

---


$$\frac{\partial f_2}{\partial \dot{q}} = \frac{\partial}{\partial \dot{q}} \left[ \underline{M^T(q)} \left[ -\underline{G(q)} - C(q, \dot{q}) \dot{q} + \underline{B(q)} u \right] \right]$$

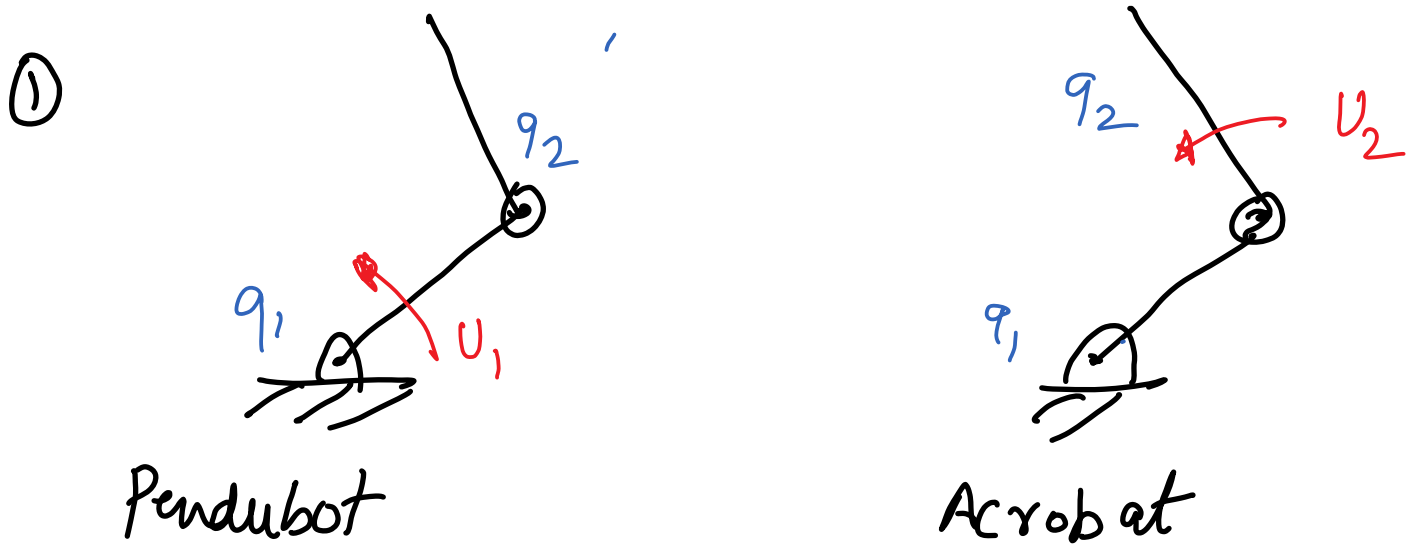
$$\hat{\Lambda} = \frac{\partial f}{\partial x} = \begin{bmatrix} 0 & I \\ -M^T \frac{\partial G}{\partial q} + \sum_j M^T \frac{\partial B_j}{\partial q} u_j & 0 \end{bmatrix}$$

$$\hat{B} = \frac{\partial f}{\partial u} =$$

$$f = \begin{bmatrix} \dot{q} \\ M^T(q) \left( -C(q, \dot{q}) \dot{q} - G(q) + B(q) u \right) \end{bmatrix}$$

$$\hat{B} = \frac{\partial f}{\partial u} = \begin{bmatrix} 0 \\ M^T(q) B(q) \end{bmatrix}$$

# Example: Underactuated Double Pendulum



Degrees of freedom = 2 ( $q_1, q_2$ )

Actuators = 1 ( $U_1$  for pendubot  
 $U_2$  for acrobot)

$$\Rightarrow U_i = -k_1 q_1 - k_2 q_2 - k_3 \dot{q}_1 - k_4 \dot{q}_2$$

$i=1$  or  $2$