

Control of manipulators

$$\frac{d}{dt} \left(\frac{\partial \mathcal{L}}{\partial \dot{q}} \right) - \frac{\partial \mathcal{L}}{\partial q} = \tau$$

↓

$$\underline{\underline{Ax = b}}$$

$$\theta = \ddot{q}$$

$$M(q) \ddot{q} + C(q, \dot{q}) \dot{q} + G(q) = \tau$$

$$\underbrace{M(q)}_A \underbrace{\ddot{q}}_X = \underbrace{\tau - C(q, \dot{q}) \dot{q} - G(q)}_b$$

→ $M(q) = \text{mass/inertia}$

$C(q, \dot{q}) \dot{q} = \text{Coriolis acceleration/torque}$

$G(q) = \text{gravitational torque}$

$\tau = \text{external torque}$

a) Set-pt. control :

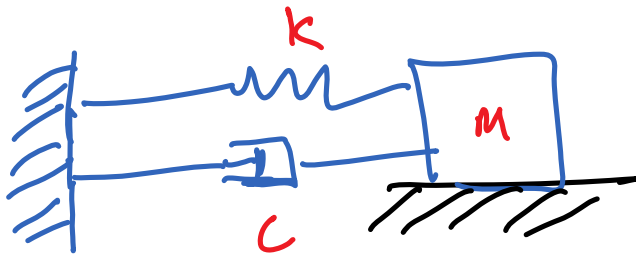
b) Trajectory control :

Simplest example:

$$M(q) \ddot{q} + C(q, \dot{q}) \dot{q} + G(q) = \tau$$

$$\downarrow \qquad \qquad \downarrow \qquad \qquad \downarrow$$
$$\underline{m} \ddot{q} + \underline{c} \dot{q} + \underline{k} q = \tau$$

spring-mass-damper system



$$\ddot{q} + \frac{c}{m} \dot{q} + \frac{k}{m} q = \frac{\tau}{m} \quad \text{free vibration}$$

$$\omega_n = \sqrt{\frac{k}{m}} ; \quad 2\zeta \omega_n = \frac{c}{m}$$

$$\downarrow$$
$$\zeta = \frac{c}{2\sqrt{mk}}$$

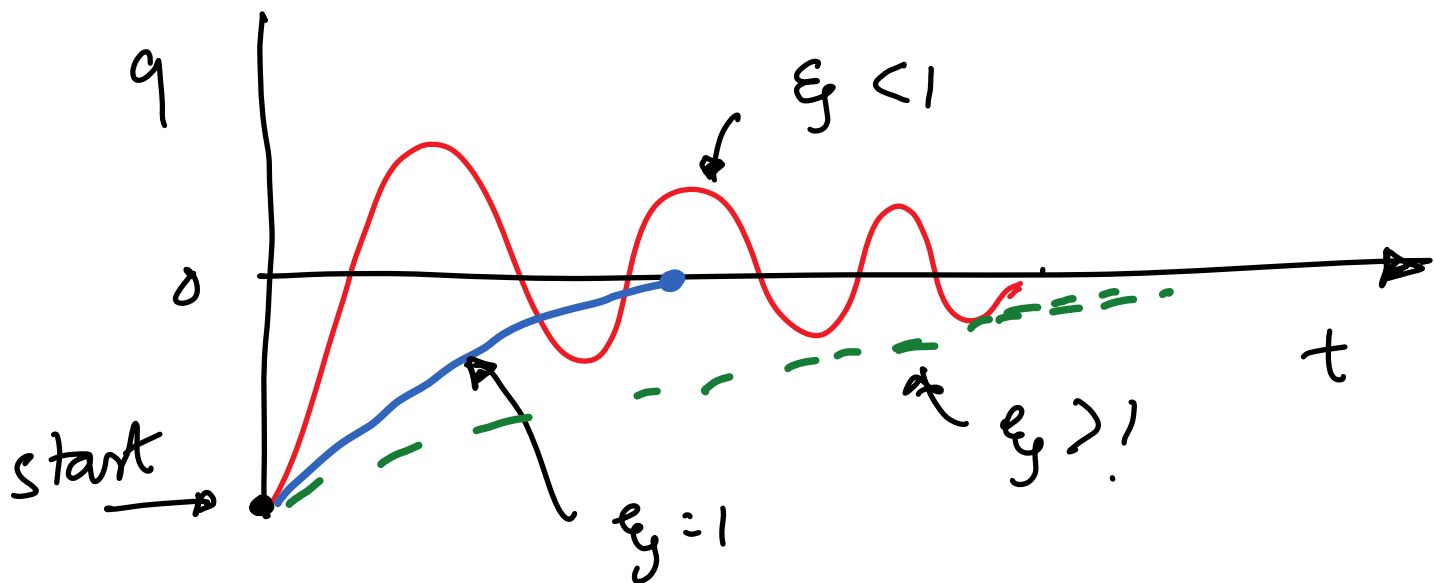
3 cases

$$\zeta = \frac{c}{2\sqrt{mk}}$$

① $\zeta > 1 \Rightarrow c > 2\sqrt{mk}$ overdamped

② $\zeta = 1 \Rightarrow c = 2\sqrt{mk}$ critically damped

③ $\zeta < 1 \Rightarrow c < 2\sqrt{mk}$ under-damped



fastest decay to zero

we will use Force /
torque to achieve
 $\zeta = 1$ to achieve

fast est damping.

$$m\ddot{q} + c\dot{q} + kq = \tau \quad \text{--- (1)}$$

$$\tau = -k_p q - k_d \dot{q} \quad \text{--- (2)}$$

↑
proportional
control

↑
derivative
control (PD control)

Put (2) in (1)

designer's choice

$$m\ddot{q} + c\dot{q} + kq = -k_p q - k_d \dot{q}$$

$$m\ddot{q} + (c + k_d)\dot{q} + (k + k_p)q = 0$$

$$(c + k_d) = 2\sqrt{m(k + k_p)} \quad \text{critically damped}$$

solve for k_d

$$\Rightarrow c^2 + 2k_d c + k_d^2 = 4mk + 4mk_p$$

$$\Rightarrow k_d^2 + 2k_d c + (c^2 - 4mk - 4mk_p) = 0$$

Solve for k_d

$$k_d = \frac{-2 \pm \sqrt{(2c)^2 - 4(l)(c^2 - 4(k+k_p)m)}}{2(l)}$$

Simplify:

$$k_d = -c \pm 2\sqrt{(k+k_p)m}$$

↓

(choose stable gain)

$$k_d = -c + 2\sqrt{(k+k_p)m}$$

$k_p, k_d \rightarrow$ designer's choice

Extend to 2-D system

$$1D \quad m\ddot{q} + c\dot{q} + kq = \tau \quad \left\| \begin{array}{l} \tau = -k_p q - k_d \dot{q} \\ \text{2} \\ \text{1 equation} \end{array} \right.$$

2D

$$\begin{bmatrix} m_{11} & m_{12} \\ m_{21} & m_{22} \end{bmatrix} \begin{bmatrix} \ddot{q}_1 \\ \ddot{q}_2 \end{bmatrix} + \begin{bmatrix} c_{11} & c_{12} \\ c_{21} & c_{22} \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix} + \begin{bmatrix} k_{11} & k_{12} \\ k_{21} & k_{22} \end{bmatrix} \begin{bmatrix} q_1 \\ q_2 \end{bmatrix} = \begin{bmatrix} \tau_1 \\ \tau_2 \end{bmatrix}$$

$$\tau = -k_p q - k_d \dot{q}$$

$$\begin{bmatrix} \tau_1 \\ \tau_2 \end{bmatrix} = - \underbrace{\begin{bmatrix} k_{p11} & k_{p12} \\ k_{p21} & k_{p22} \end{bmatrix}}_4 \begin{bmatrix} q_1 \\ q_2 \end{bmatrix} - \underbrace{\begin{bmatrix} k_{d11} & k_{d12} \\ k_{d21} & k_{d22} \end{bmatrix}}_4 \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix}$$

8 free parameters

2 conditions (critical damping)

Feedback Linearization / control partitioning

$$\textcircled{1} M \ddot{q} + C(q, \dot{q}) \dot{q} + G(q) = \tau$$

$$\textcircled{2} \text{ Choose } \tau = \hat{M}(-k_p q - k_d \dot{q}) + \hat{C}(q, \dot{q}) \dot{q} + \hat{G}(q)$$

$\hat{M}, \hat{C}, \hat{G} \rightarrow$ estimates of M, C, G

Let's assume $M = \hat{M}; C = \hat{C}; G = \hat{G}$

Substitute $\textcircled{2}$ in $\textcircled{1}$

$$M \dot{q} + C(q, \dot{q}) \dot{q} + G(q) = M(-k_p q - k_d \dot{q}) + C(q, \dot{q}) \dot{q} + G(q)$$

$$M(\ddot{q} + k_d \dot{q} + k_p q) = 0$$

Since $M \neq 0 \quad \ddot{q} + k_d \dot{q} + k_p q = 0$

$$\begin{bmatrix} \ddot{q}_1 \\ \ddot{q}_2 \\ \vdots \\ \ddot{q}_n \end{bmatrix} + \begin{bmatrix} k_{d1} & 0 & 0 & \dots \\ 0 & k_{d2} & 0 & \dots \\ 0 & 0 & k_{d3} & \dots \\ \dots & \dots & \dots & k_{dn} \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \\ \dot{q}_3 \\ \vdots \\ \dot{q}_n \end{bmatrix} + \begin{bmatrix} k_{p1} & 0 & 0 & \dots \\ 0 & k_{p2} & 0 & \dots \\ 0 & 0 & k_{p3} & \dots \\ 0 & 0 & \dots & k_{pn} \end{bmatrix} \begin{bmatrix} q_1 \\ q_2 \\ \vdots \\ q_n \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ \vdots \\ 0 \end{bmatrix}$$

$$\ddot{q}_1 + k_{d1} \dot{q}_1 + k_{p1} q_1 = 0$$

$$\ddot{q}_2 + k_{d2} \dot{q}_2 + k_{p2} q_2 = 0$$

⋮

$$\ddot{q}_n + k_{dn} \dot{q}_n + k_{pn} q_n = 0$$

n equations

$$k_d = -c + 2\sqrt{m(k+k_p)}$$

$$m\ddot{q} + c\dot{q} + kq = z$$

$$m\ddot{q} + (c+k_d)\dot{q} + (k+k_p)q = 0$$

$$c = 0 ; m = 1 ; k = 0$$

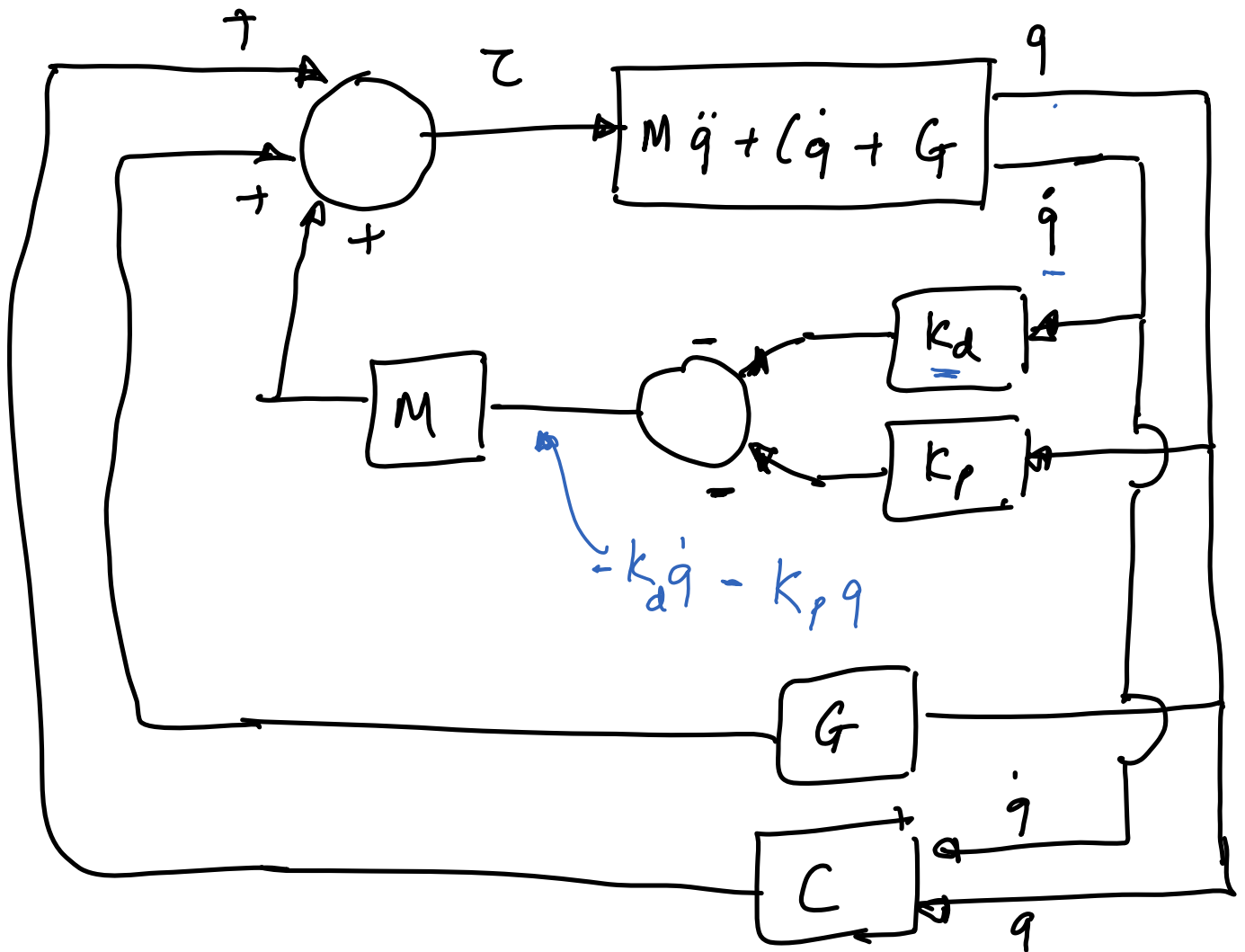
$$k_{di} = 0 + 2\sqrt{(1)(0 + k_{pi})}$$

$$k_{di} = 2\sqrt{k_{pi}}$$

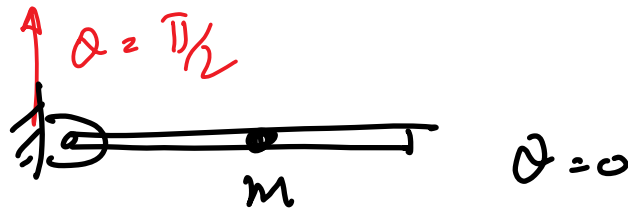
$$\textcircled{1} M\ddot{q} + c(q, \dot{q})\dot{q} + G(q) = \tau$$

$$\textcircled{2} \text{ Choose } \tau = \hat{M}(-k_p\dot{q} - k_d\ddot{q}) + \hat{C}(q, \dot{q})\dot{q} + \hat{G}(q)$$

Block diagrams



Example: 1-Link pendulum



Start: $\theta = 0$

End: $\theta = \pi/2$

$$M(q) \ddot{q} + C(q, \dot{q}) \dot{q} + G(q) = \tau$$

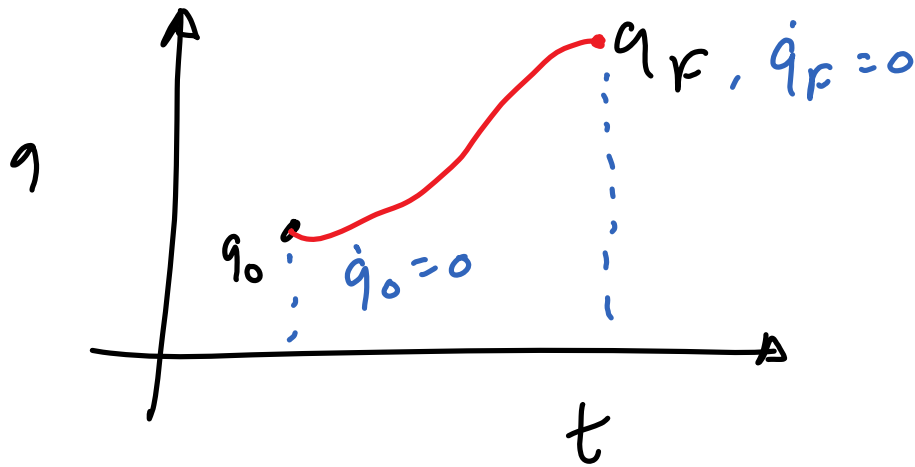
$$ml^2 \ddot{\theta} + 0 + mgl \sin(\theta) = \tau$$

Controllers

$$\textcircled{1} \quad \tau = -k_p (q - q_d) - k_d \dot{q} \quad \begin{array}{l} q_d = \\ \text{reference} \\ = \pi/2 \end{array}$$

$$\textcircled{2} \quad \tau = \underbrace{M(-k_p (q - q_d) - k_d \dot{q})}_{ml^2} + \underbrace{C(q, \dot{q}) \dot{q}}_0 + \underbrace{G(q)}_{mgl \sin \theta}$$

Feedback linearization for trajectory tracking



$$q_{\text{ref}}(t) = a_0 + a_1 t + a_2 t^2 + a_3 t^3$$

Dynamics : $\underline{M\ddot{q} + C\dot{q} + G} = \underline{z}$

Control : $\underline{z = M(\ddot{q}_{\text{ref}} - k_d(\dot{q} - \dot{q}_{\text{ref}}) - k_p(q - q_{\text{ref}}))} + G + C\dot{q}$

$$\underline{M\ddot{q}} = \underline{M(\ddot{q}_{\text{ref}} - k_d(\dot{q} - \dot{q}_{\text{ref}}) - k_p(q - q_{\text{ref}}))}$$

$$M(\underbrace{\ddot{q} - \ddot{q}_{\text{ref}}}_{\dot{e}_{\text{ref}}}) + k_d(\underbrace{\dot{q} - \dot{q}_{\text{ref}}}_{\dot{e}_{\text{ref}}}) + k_p(\underbrace{q - q_{\text{ref}}}_{e}) = 0$$

\dot{e}_{ref}

\dot{e}_{ref}

e

$$\underline{M} \ddot{q} = M (\ddot{q}_{\text{ref}} - k_d (\dot{q} - \dot{q}_{\text{ref}}) - k_p (q - q_{\text{ref}}))$$

$$M (\ddot{q} - \ddot{q}_{\text{ref}} + k_d (\dot{q} - \dot{q}_{\text{ref}}) + k_p (q - q_{\text{ref}})) = 0$$

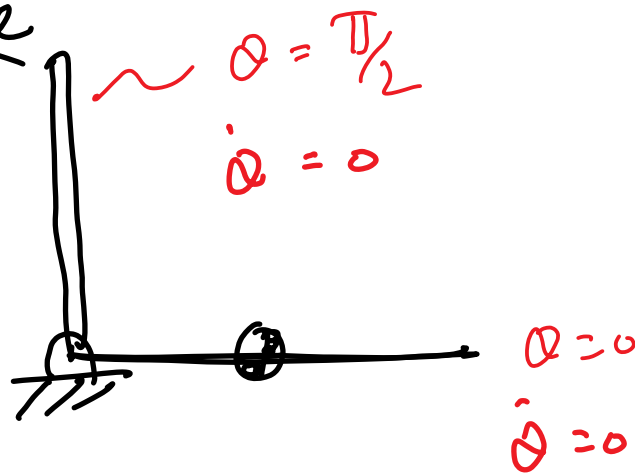
$\underbrace{\quad}_{\ddot{e}}$
 $\underbrace{\quad}_{\dot{e}}$
 $\underbrace{\quad}_{e}$

$$M \ddot{e} + k_d \dot{e} + k_p e = 0$$

~ Spring-mass-damper

Block diagram

Example



$$q_{\text{ref}}(t) = a_0 + a_1 t + a_2 t^2 + a_3 t^3$$

Feedback Linearization in Task space

→ So far $q_{ref}, \dot{q}_{ref}, \ddot{q}_{ref}$ $q = \text{joint position}$

→ $z = M(\ddot{q}_{ref} - k_d(\dot{q} - \dot{q}_{ref}) - k_p(q - q_{ref})) + C + G$

(II)

→ What if $\begin{matrix} x_{ref}, \dot{x}_{ref}, \ddot{x}_{ref} \\ y_{ref}, \dot{y}_{ref}, \ddot{y}_{ref} \end{matrix}$ } same ideas to projector

→ $z = \begin{matrix} ? \\ 0 \\ 1 \end{matrix}$

$\begin{Bmatrix} x \\ y \end{Bmatrix} \Rightarrow X = f(q)$

↑ forward kinematics

$x_{ref} = f(q_{ref})$

$q_{ref} = f^{-1}(x_{ref})$

Inverse kinematics (using fsolve)

(I)

$$\dot{X} = \frac{\partial f}{\partial q} \dot{q} \quad \dot{X}_{\text{ref}} = J \dot{q}_{\text{ref}}$$

$\parallel J$

$$\dot{q}_{\text{ref}} = J^{-1} \dot{X}_{\text{ref}} \quad \text{--- (I)}$$

$$\dot{X} = J \dot{q}$$

$$\ddot{X} = \frac{dJ}{dt} \dot{q} + J \ddot{q}$$

$$\ddot{X} = \dot{J} \dot{q} + J \ddot{q}$$

$$\ddot{X}_{\text{ref}} = \dot{J} \dot{q}_{\text{ref}} + J \ddot{q}_{\text{ref}}$$

$$\ddot{q}_{\text{ref}} = J^{-1} (\ddot{X}_{\text{ref}} - \dot{J} \dot{q}_{\text{ref}}) \quad \text{--- (II)}$$

Given $\ddot{X}_{\text{ref}}, \dot{X}_{\text{ref}}, X_{\text{ref}}$. Compute

$\ddot{q}_{\text{ref}}, \dot{q}_{\text{ref}}, q_{\text{ref}}$ using (I), (II), (III)

Z from (IV)