

① Set-point control

$$\rightarrow M \ddot{\theta} + C(\theta, \dot{\theta})\dot{\theta} + G(\theta) = Z$$

$$\rightarrow \text{set-point } \theta = \underline{\underline{\theta_d}}$$

2 options

$$\rightarrow ① \quad Z = -k_p(\theta - \theta_d) - k_d \dot{\theta} \quad (\text{Coppelia sim})$$

$$\rightarrow ② \quad \underline{Z} = M(-k_p(\theta - \theta_d) - k_d \dot{\theta}) + \underline{C(\theta, \dot{\theta})} + \underline{G(\theta)}$$

$$\left| \begin{array}{l} \text{in decoupled system} \\ k_d = z\sqrt{k_p} \end{array} \right.$$

examples

(i) random / fictitious $2 \times L$

(ii) single link pendulum

a) P-D ①

b) control partitioning ②

Trajectory tracking

$\ddot{\alpha}_{ref}$, $\dot{\alpha}_{ref}$, α_{ref} (e.g. fifth order polynomial)

$$\tau = M \left(\ddot{\alpha}_{ref} - k_p(\alpha - \alpha_{ref}) - k_d(\dot{\alpha} - \dot{\alpha}_{ref}) \right) + C(\alpha, \dot{\alpha})\dot{\alpha} + G(\alpha) \quad \text{--- (1)}$$

$$M \ddot{\alpha} + C(\alpha, \dot{\alpha})\dot{\alpha} + G(\alpha) = \tau \quad \text{--- (2)}$$

put (1) in (2)

$$\Rightarrow M \ddot{\alpha} + C(\alpha, \dot{\alpha})\dot{\alpha} + G(\alpha) = M (\ddot{\alpha}_{ref} - k_p(\alpha - \alpha_{ref}) - k_d(\dot{\alpha} - \dot{\alpha}_{ref})) + C(\dot{\alpha}, \ddot{\alpha}) + G(\alpha)$$

$$\Rightarrow M \left[(\ddot{\alpha} - \ddot{\alpha}_{ref}) + k_p(\alpha - \alpha_{ref}) + \underline{k_d(\dot{\alpha} - \dot{\alpha}_{ref})} \right] = 0$$

$$e = \alpha - \alpha_{ref}$$

$$\Rightarrow M \left[\underbrace{\ddot{e} + k_d \dot{e} + k_p e}_{\text{spring-mass-damper}} \right] = 0$$

$$k_d = 2\sqrt{k_p}$$

Alternate

$$\rightarrow \tau = -k_p(\alpha - \alpha_{ref}) - k_d(\dot{\alpha} - \dot{\alpha}_{ref}) \quad \leftarrow$$

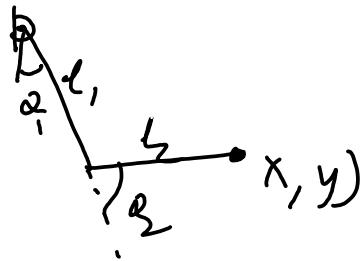
Naive P-D controller

(3) Cartesian-based tracking

$$q = \{x, y\}$$

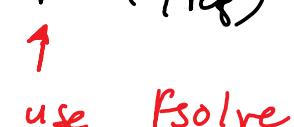
$$q_{ref} = \{x_{ref}, y_{ref}\}$$

$q_{ref}, \dot{q}_{ref}, \ddot{q}_{ref}$  given



Forward kinematics : $\checkmark q_{ref} = f(\theta_{ref})$  

Inverse kinematics : $\checkmark \theta_{ref} = F^{-1}(q_{ref})$



Differentiate eq =  $\dot{q}_{ref} = \frac{dF}{d\theta}(\theta_{ref})$

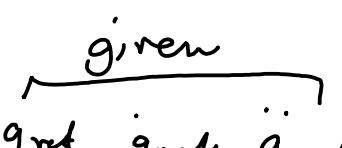
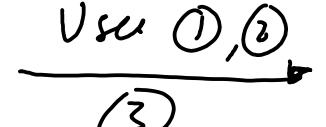
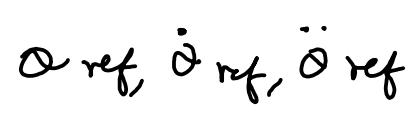
$$\dot{q}_{ref} = J \dot{\theta}_{ref} \quad \left(J = \frac{\partial F}{\partial \theta} \right) \quad \text{(II)}$$

 - $\ddot{q}_{ref} = (J^{-1}) \ddot{q}_{ref}$

Differentiate  $\dot{q}_{ref} = J \ddot{\theta}_{ref} + J \dot{\theta}_{ref}$

$$\ddot{\theta}_{ref} = J^{-1} \{ \ddot{q}_{ref} - J \dot{\theta}_{ref} \}$$



Stage 1 given

$$\underline{\dot{q}_{ref}, \ddot{q}_{ref}, \ddot{\dot{q}}_{ref}} \xrightarrow[\textcircled{3}]{\text{use } \textcircled{1}, \textcircled{2}} \underline{\alpha_{ref}, \dot{\alpha}_{ref}, \ddot{\alpha}_{ref}}$$

Stage 2

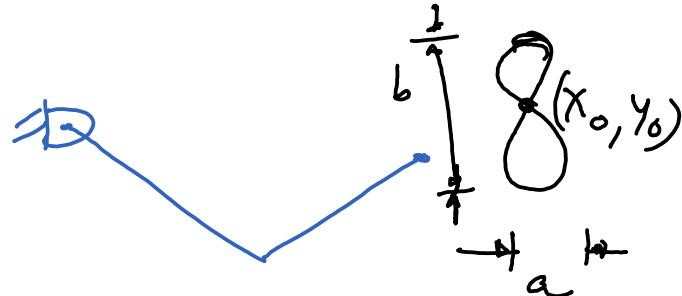
$$Z = M \left[\ddot{\alpha}_{ref} - k_p (\alpha - \alpha_{ref}) - k_d (\dot{\alpha} - \dot{\alpha}_{ref}) \right] + C(\alpha, \dot{\alpha}) \dot{\alpha} + G(\alpha)$$

Example

$$\rightarrow x = x_0 + A \sin(aZ)$$

$$\rightarrow y = y_0 + B \cos(bZ)$$

$$q = \{x, y\}$$



Lemniscate

$$q_{ref} = ? \quad Z = 0, 2\pi$$

$$(x_{ref}, y_{ref}) \quad \stackrel{?}{=} Z$$

$$\dot{x} = A a \cos(aZ) \frac{dZ}{dt} \quad \dot{x} = 0 \quad \stackrel{?}{=} 0$$

$$\dot{y} = -B b \sin(bZ) \frac{dZ}{dt} \quad \dot{y} = 0 \quad \stackrel{?}{=} 0$$

$$\ddot{x} = -A a \sin(aZ) \frac{d^2Z}{dt^2} \quad \ddot{x} = 0 \quad \stackrel{?}{=} 0$$

$$\ddot{y} = -B b \cos(bZ) \frac{d^2Z}{dt^2} \quad \ddot{y} = 0 \quad \stackrel{?}{=} 0$$

$\tau = 0, 2\pi$ x_{ref}, y_{ref} start, end position
 $\dot{z} = 0$ at $\tau = 0, 2\pi$ $\dot{x}_{ref}, \dot{y}_{ref} = 0$ "
 $\ddot{z} = 0$ at $\tau = 0, 2\pi$ $\ddot{x}_{ref}, \ddot{y}_{ref} = 0$ "
 $z = \underline{a_0} + \underline{a_1} t + \underline{a_2} t^2 + \underline{a_3} t^3 + \underline{a_4} t^4 + \underline{a_5} t^5$
 6 conditions & 6 constants

Find a's

$x_{ref}, y_{ref}, \dot{x}_{ref}, \dot{y}_{ref}, \ddot{x}_{ref}, \ddot{y}_{ref}$ ✓

Control schemes

$$M(\theta) \ddot{\theta} + C(\theta, \dot{\theta}) \dot{\theta} + G(\theta) = Z$$

① P-I-D control

$$Z = -k_p(\theta - \theta_{ref}) - k_d(\dot{\theta} - \dot{\theta}_{ref}) - k_i \int (\theta - \theta_{ref}) dt$$

② Control partitioning

$$Z = M(\theta) [\ddot{\theta}_{ref} - k_p(\theta - \theta_{ref}) - k_d(\dot{\theta} - \dot{\theta}_{ref})] + \underbrace{C(\theta, \dot{\theta}) \dot{\theta} + G(\theta)}_{\text{Sensor measurement}}$$

③ Feed Forward

$$Z = Z_{ff} - k_p(\theta - \theta_{ref}) - k_d(\dot{\theta} - \dot{\theta}_{ref})$$

$$Z_{ff} = \underbrace{M(\theta_{ref}) \ddot{\theta}_{ref} + C(\theta_{ref}, \dot{\theta}_{ref}) \dot{\theta}_{ref} + G(\theta_{ref})}_{\text{pre-computed}}$$

④ P-D + gravity compensation

$$Z = \underbrace{-k_p(\theta - \theta_{ref}) - k_d(\dot{\theta} - \dot{\theta}_{ref})}_{\text{}} + G(\theta)$$

good when manipulator is in vertical plane & moving slowly.

When manipulator moves fast $C(\theta, \dot{\theta}) \dot{\theta}$ is substantially

~~substantially~~

